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Gate leakage reduction in AlGaN/GaN HEMTs using in situ ion treatment

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Abstract

A new in situ treatment method is proposed to reduce the gate leakage in normally-on AlGaN/GaN HEMTs. It consists of O_2 -Ar ion bombardment before the gate metalization. Ion treatment is found to improve the quality of gate metal and semiconductor interfaces. This process reduces the gate leakage current by around 25 times. The process is validated for wafer level uniformity and temperature dependency against the traditional NH₄OH treatment. Ion treated HEMT devices are found to possess two orders of magnitude smaller standard deviations in gate leakage distribution across the wafer. The gate leakage is found to be less dependent on temperature comparatively. The trap energy level of the HEMTs treated using the proposed method is found to be higher than the traditional ones as extracted from Poole-Frenkel electron emission analysis. The new method results in a 0.13 dB improvement in the minimum noise figure of the HEMT on average from DC—16 GHz.

1. Introduction

The microwave community prefers designing transmitter, receiver, and transceiver circuits using Gallium Nitride (GaN) technology. GaN high electron mobility transistor(HEMT) emerged as a promising candidate for space, defense, and commercial applications[[1](#page-10-0)–[5](#page-10-0)]. Important attributes associated with GaN HEMTs are superior power density, high efficiency, promising thermal conductivity, enhanced saturated carrier velocity, and high electrical breakdown [[6](#page-10-0)–[8](#page-10-0)]. These benefits have led to rich research and literature on GaN-based power amplifiers. GaN HEMT technology offers low noise amplifiers that are faster, stronger, and more durable than their GaAs counterparts, negating the need for a limiter after the receiver antenna in the front-end assembly [[9](#page-10-0)–[12](#page-10-0)]. Silicon Carbide (SiC) is a preferred choice as a substrate for power performance due to its high thermal conductivity [[13,](#page-10-0) [14](#page-10-0)].

One of the important factors to influence the device performance is the gate leakage current. Despite the advantages of AlGaN/GaN HEMTs and surpassing other III-V counterparts to achieve the required Johnson figure of merit [[15](#page-10-0)], these devices are limited by gate leakage current [[16](#page-10-0)–[23](#page-10-0)]. The gate leakage also leads to the current collapse phenomenon related to surface state trapping in AlGaN/GaN HEMTs[[24](#page-10-0)]. High gate leakage current results in the degradation of noise performance and breakdown voltage reduction [[25](#page-10-0)].

Low leakage current is essential for applications that require low noise levels. Several methods are developed for leakage current reduction in GaN HEMTs. These methods are mainly related to in situ/ex-situ treatment before passivation layer[[26](#page-10-0)], passivation layer schemes[[27](#page-10-0)], treatment before gate metal deposition [[28](#page-10-0)], gate metal stack variation [[29](#page-10-0)], and adding an insulator to have MIS-HEMT structure [[30](#page-10-0)]. The main motivation of these methods is to improve surface passivation at the access region, to improve metal/semiconductor interface

quality, or to put an additional barrier under the gate to minimize the injection of electrons from the gate to twodimensional electron gas(2DEG).

This paper demonstrates the effect of $O₂$ -Ar ion process treatment before gate metal deposition. It effectively reduces the gate leakage current by 25 times with high wafer level uniformity without degrading the DC and RF performance of the device. The HEMT fabrication process, along with the details of novel treatment before gate metal deposition, is discussed in section II. Section III explains wafer level performance with and without the newly introduced ion treatment step and gate leakage current dynamics. DC and RF performance of the device is summarized in section IV, while a conclusion is provided in section V.

2. HEMT fabrication

SiC is the most suitable substrate for the GaN HEMT fabrication because of a better lattice match with GaN and higher thermal conductivity compared to that of Silicon (Si). A heterostructure is formed by an AlGaN layer on top of the channel GaN layer to create the mismatch to utilize piezoelectric polarization, which forms a 2DEG consisting of free electrons with high mobility. The devices investigated in this submission are fabricated using NANOTAM's 0.15 μm GaN-on-SiC HEMT technology. An epi-layer containing 20 nm AlGaN and a 3 nm GaN cap layer is grown on a 3-inch GaN-on-SiC wafer with metal organic chemical vapor deposition. The purpose of

the thin GaN cap layer is to eliminate the oxidation of Al in the AlGaN layer, resulting in lower surface defects and higher reliability [[31](#page-10-0)]. The measured 2DEG low field mobility and 2DEG concentration are 1960 cm $^2/\mathrm{Vs}$ and [1](#page-2-0).20x10 13 cm $^{-2}$, respectively. The process flow and simplified device geometry are shown in figure 1(a). The device has a 150 nm gate length (L_g), a 3 μ m drain-source distance and a gate in the middle of drain-source contacts. For power amplifiers, gate is put near to source (away from drain) to increase breakdown voltage [[32](#page-11-0)]. For LNAs, this asymmetric gate configuration is not required. The gate-source distance (L_{gs}) is 1.425 μ m. The developed treatment method is compared with well-known NH₄OH treatment regarding DC and RF performance.

The fabrication steps are ohmic contact formation, mesa isolation, deposition of the first passivation layer, T-gate formation, creation of the first metal layer, deposition of second passivation, and the second metal layer. Ohmic contacts are formed by rapid thermal annealing of Ti/Al/Ni/Au metal stack. The contact resistance and sheet resistance from transfer length method measurements is 0.4 Ω/mm and 280 Ω/\square , respectively. The first Silicon Nitride (SiN) passivation is deposited by plasma-enhanced chemical vapor deposition to passivate the dangling bonds at the semiconductor surface. To have a T-shaped gate contact, the first passivation layer is etched by F-based (CHF₃, CF₄, and SF₆) reactive ion etching with a low power to avoid damage to the GaN surface. The T-shaped gate contact is formed with e-beam lithography (EBL) and e-beam evaporator systems. The first metal layer is created by lift-off technique with 1.1 μ m Ti/Au metal stack. The second passivation and the second metal layers are formed using the methods employed for their corresponding first layers. If the passivation processes can suppress surface leakage currents, metal-semiconductor junctions dominate gate leakage. Therefore, the treatment before gate metal deposition turns out to be crucial.

We introduce the O₂-Ar ion process before gate metal deposition as a novel crucial step shown in figure [1](#page-2-0)(a) with a filled circle. Initially, O_2 ions are sent to the sample's surface to remove organic residues from EBL resist. After that, Ar ions are used to remove the oxidized layer from the surface physically. In that way, carbon contamination and poor quality thin oxidized surfaces are successfully removed. This in situ treatment effectively increases the Schottky junction quality. Figure [1](#page-2-0)(b) shows the SEM image of $4 \times 75 \,\mu m$ HEMT after

successful fabrication. The band diagram in figure $2(a)$ $2(a)$ is showing the 2DEG formation between AlGaN and GaN buffer. CV curve shown in figure [2](#page-3-0)(b) explains the existence of 2DEG and also depletion of 2DEG with negative gate bias. From CV characteristics, pinch-off voltage of the ion treated and NH4OH treated device are -4.2 V and -3.5 V, respectively. It is to be mentioned that the O_2 -Ar ion treatment is commonly used to remove organic contamination coming from photoresist residue [[33](#page-11-0)–[36](#page-11-0)]. This is the first time, to the best of the authors' knowledge, that O_2 -Ar ion treatment is introduced in the literature before gate metal deposition. It reduces gate leakage current without significant degradation in the device performance and increases the uniformity of the leakage current throughout the wafer.

3.Wafer level performance and gate leakage dynamics

Generally, the leakage current of single HEMTs is studied in the literature, but the leakage current may vary depending on the chip's position within the wafer. Thus, assessing the leakage current distribution across the wafer helps to examine the method's suitability for wafer production. Figure [3](#page-3-0) shows the gate leakage current of multiple devices through which the distribution of the leakage currents across the entire wafer is studied.

Table [1](#page-5-0) indicates that the ion treatment suppresses the gate leakage current more than one order of magnitude, and it has two orders of magnitude smaller standard deviation. Figure 4 compares the absolute value of the gate leakage between an ion treated and NH4OH treated device. In both treatment methods, the gate leakage current is larger than the drain leakage current at the drain voltages between 0 V and 40 V under -8 V gate bias. This shows that the leakage current between drain-source contacts due to high drain bias is much less than that of between reverse bias gate-source Schottky junction.

Table 1. Gate leakage current statistics of 4 \times 75 $\,\mu{\rm m}$ HEMTs at 25° C.

It can be seen in figure [5](#page-4-0) that there is a significant reduction in the gate leakage current above the threshold voltage (V_t) . The drain and source are grounded to eliminate drain bias dependency of leakage current. To clarify the gate leakage dynamics for these two treatment methods, gate leakage measurements are taken at several temperatures ranging from 25 °C to 150 °C. Figure 6 shows the temperature dependence of the gate leakage at different gate reverse bias levels for ion and NH₄OH treated device. As temperature rises, the gate leakage current of the NH₄OH treated device initially increases for the gate bias above V_t . However, it is observed that elevating the temperature at gate voltage higher than the V_t results in a slight reduction in the leakage current. In the case of an ion treated device, the minimum leakage current occurs at a gate voltage above V_t , specifically when the temperature is around 75 °C. This behavior is related to deep acceptor trap initiated impact ionization [[20](#page-10-0)]. The gate leakage current consistently increases with rising temperature for temperatures exceeding 75 °C and gate voltages below V_t . It is noticeable that leakage in ion treatment is less dependent on temperature as it has lower variation as a function of temperature.

The reverse bias gate current in GaN HEMTs is separated into four distinct elements: thermionic emission, trap-assisted tunneling, Poole-Frenkel (PF) emission, and Fowler-Nordheim tunneling [[37](#page-11-0)]. Since the gate length of the device is as small as 150 nm, there will be a considerable uneven distribution of leakage current

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Table 2. $4 \times 75 \ \mu m$ HEMTs parameters from small signal and noise measurements.

density under the gate [[38](#page-11-0)]. Therefore, only PF emission analysis will be provided, and the method used is similar to that in [[39](#page-11-0)]. As a difference in [[39](#page-11-0)], the electric field is obtained from simulations in Silvaco ATLAS TCAD. The relationship between leakage current density (J_{leak}) and electric field (E) is given by [[39](#page-11-0)]

$$
J_{leak} \approx J_{PF} = CExp \left[-\frac{q(\phi_t - \sqrt{(qE/\pi\epsilon_s)})}{kT} \right],
$$
 (1)

where C is a constant, ϕ_t is the barrier height for electron emission from the trap state, and ϵ_s is the permittivity of the semiconductor at high frequency. After rearranging equation (1)

$$
ln(J_{leak}/E) = \frac{q}{kT} \sqrt{\frac{qE}{\pi \epsilon_s}} + c(T),
$$
\n(2)

where

$$
c(T) = -\frac{q\phi_t}{kT} + \ln(C) \tag{3}
$$

Figure [7](#page-6-0) shows the plot of equation (2), valid for gate voltage above the V_t . The barrier height for electron emission from the trap state is extracted as 0.27 eV and 0.46 eV for NH₄OH treated and ion treated devices, respectively. Figure [8](#page-6-0) shows that the ion treated device has a higher barrier for electron emission.

4. DC and RF characterizations of HEMTs

HEMT periphery and topology both have significance in the design of a monolithic microwave integrated circuit (MMIC) amplifiers. Small periphery devices are suitable for low noise, high gain, and high frequency applications, while large periphery devices are favorable for high power and low frequency applications. Therefore, an optimum periphery is always chosen for particular amplifier design requirements. In this writing, DC and small signal performance of a 4 \times 75 μ m small periphery HEMT is analyzed focussing low noise amplifier design involving NH4OH and ion treatment fabrications.

DC measurements of $4 \times 75 \mu m$ HEMT provides technology figures-of-merit. The maximum drain current (I_{Dmax}) of 1.11 A/mm at Vgs = 1 V and maximum transconductance $(g_{\text{m,max}})$ of 326 mS/mm are found for NH₄OH process while for ion treatment, these values are 1.14 A/mm and 329 mS/mm. The breakdown voltage

at Ig $=1 \text{ mA/mm}$ is 40 V, the same for both fabrications. This shows that HEMTs have similar DC performance from both processes.

Small signal measurements of HEMTs from NH4OH and ion treatments are performed on Rohde & Schwarz ZVA PNA up to 40 GHz using external bias tees on-wafer. The measurements are performed under bias conditions of 10 V and 150 mA/mm. The 10 V is the external voltage, and 150 mA/mm is 13 % of I_{Dmax} . Data for the 4 \times 75 μ m HEMTs are recorded, and HEMT's performance parameters are extracted using PathWave Advanced Design System (ADS) from Keysight Technologies. These parameters include HEMT's input capacitance (C_{in}), output capacitance (C_{out}), and drain-source resistance (R_{ds}). Input reflection coefficient (IRL) of HEMT provides C_{in}, output reflection coefficient (ORL) gives C_{out} and R_{ds}. The other parameters include maximum available gain (MAG), maximum stable gain (MSG), cut-off frequency (f_t) , and maximum oscillation frequency (f_{max}) .

Figure [9](#page-6-0) shows C_{in} and C_{out} of the HEMTs from NH₄OH treatment and ion treatment. Input impedance has capacitive behavior up to 30 GHz and becomes inductive after that. The capacitance values are almost the same, up to 15 GHz for both processes and after that, ion treatment capacitance starts to increase. Figure [10](#page-7-0) shows R_{ds} of the HEMTs from NH4OH treatment and ion treatment. NH4OH treatment has comparatively higher resistance than ion treatment. Lower R_{ds} results in the reduction of gain.

The technology figures-of-merit f_t and f_{max} of the $4 \times 75 \mu$ m HEMTs are characterized using small signal measurement data by extrapolating the current gain and MAG curves. It can be seen from linear fitting in figures [11](#page-7-0) and [12](#page-7-0) that f_t and f_{max} values for NH₄OH treatment are 55 GHz and 63 GHz, respectively, while corresponding values for ion treatment are 52 GHz and 64 GHz. Although it appears from figures [11](#page-7-0) and [12](#page-7-0) that f_{t} and f_{max} values are slightly higher for ion treatment, it is justified to conclude that both treatment have almost same values of f_t and f_{max} .

Gate leakage current is in direct relevance with the noise performance of the HEMT [[25](#page-10-0)]. Minimum noise figure (NF $_{\rm min}$) of both NH₄OH treated and ion treated HEMTs is measured as shown in figure [13.](#page-8-0) Owing to the lower gate leakage current, the noise performance of the device fabricated using the novel ion treatment method is far better than NH4OH treatment. Therefore, it is justified to claim that the devices fabricated using the proposed method are promising for GaN-based low noise amplifiers.

Table [2](#page-8-0) summarizes the small signal parameters of HEMTs fabricated using both NH4OH and ion treatment techniques. All parameter values are shown at 10 GHz except f_t and f_{max} . It is observed that ion treatment results in a decrease of MAG, C_{in} , R_{ds} and f_t . f_{max} and NF $_{min}$ are improved. C_{out} is almost unchanged. The change in C_{in} value will only shift the optimum source impedance ($\Gamma_{\rm{Sopt}}$) without affecting HEMT's NF _{min} value. Similarly, the change in C_{out} and R_{ds} values will result in the shift of optimum load impedance (Γ_{Lopt}) without affecting its maximum output power.

5. Conclusion

This paper discusses a novel approach to suppress gate leakage in AlGaN/GaN HEMTs. To the best of the authors' knowledge, ion treatment is applied before the gate metal deposition for the first time. DC and RF performance of the HEMTs with traditional NH₄OH treatment and proposed $O₂$ -Ar ion treatment is observed, and there is no significant degradation. There is a shift in input and output capacitances of the HEMT with the ion treatment method, which only shifts optimum source and load impedances without affecting optimum noise and output power performance. However, gate leakage is reduced significantly. The noise performance of GaN HEMT is highly dependent on the gate leakage. Therefore, the proposed approach benefits GaN HEMTs for low noise applications.

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Data availability statement

The data cannot be made publicly available upon publication because they are not available in a format that is sufficiently accessible or reusable by other researchers. The data that support the findings of this study are available upon reasonable request from the authors.

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