

A MATHEMATICAL MODEL FOR URBAN STORM  
DRAINAGE SYSTEM DESIGN

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by  
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May 1981

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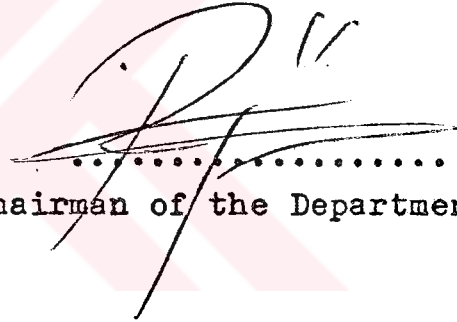
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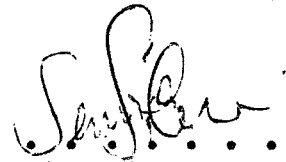
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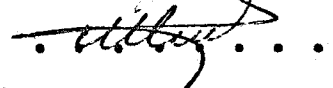
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## ABSTRACT

### A MATHEMATICAL MODEL FOR URBAN STORM DRAINAGE SYSTEM DESIGN

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M.S. in C.E.

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A hydraulic design model is developed for urban storm drainage systems. The objective of the model is to determine the required number and locations of gutter inlets, section sizes and slopes of both sewers and collectors in a drainage system. Since the failure of different elements in a storm drainage system causes different magnitudes of flood damages, the elements of the system are designed considering design storms of different periods. In the model, gutter inlets and street sewers are designed for a rainstorm of a small return period, and collectors are designed considering a more severe rainstorm by simulating the hydraulic response of previously designed elements. A hydrograph time-lag method is adopted for gutter, sewer and collector flows. Also a simplified kinematic-wave routing method is provided for sewer and collector flows as an option. Additional options concerning cross-section types of sewer and collectors; number of sewers under a street are provided in the model. A computer program in FORTRAN IV language is developed. The model is applied by using both sewer and collector flow routing schemes to an approximately 29.3 ha basin in the Bati-kent Satellite Town near Ankara. These applications illustrate the use of the mathematical model developed and also provide a comparison of the two routing schemes.

Key words : urban storm drainage, sewer, flow routing,  
hydraulic design.

## ÖZET

### KENTSEL ALANDA YAĞMURSUYU DRENAJ SİSTEM TASARIMI İÇİN MATEMATİKSEL MODEL

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Kentsel alanda yağmursuyu drenaj sistemi için hidrolik tasarım modeli geliştirildi. Modelin amacı yağmursuyu ızgaralarının yerlerinin ve sayısının belirlenmesi, sokak mecralarının ve kollektörlerin eğimlerinin ve boyutlarının hesaplanmasıdır. Sistemde elemanların değişik tekerrür süreli yağışlardaki yetersizlikleri değişik oranlarda sel hasarlarına sebep olması nedeniyle elemanların tasarımı değişik tekerrür süreli yağışlar için yapılmaktadır. Modelde yağmursuyu ızgaralarının ve sokak mecralarının küçük tekerrür süreli bir yağış için; kollektörlerin ise uzun tekerrür süreli bir yağış için tasarımı yapılmaktadır. Hendek, sokak mecrası ve kollektör akımları için hidrograf kaydırma metodu, öteleme yöntemi olarak uygulanmış ayrıca basitleştirilmiş kinematik-dalga metodu sokak mecrası ve kollektör akımları için seçenek olarak sağlanmıştır. Diğer ek seçenekler, bir sokaktaki mecra sayısı, sokak mecraları ve kollektörler için kesit tiplerinin tercih imkanıdır. Model için FORTRAN IV dilinde bir bilgisayar programı geliştirilmiş; Ankara yakınında Batıkent'te 29.3 ha lık bir havzaya uygulanmıştır. Bu uygulamalar her iki öteleme yöntemini karşılaştırmakta ve modelin kullanılmasını açıklamaktadır.

Anahtar kelimeler : Kentsel alanda yağmursuyu drenajı,  
mecra, akım ötelemesi, hidrolik tasarım.

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## NOMENCLATURE

- A : Flow area, also basin area in Table 2.1,  
A<sub>i</sub>: Subcatchment area of an inlet,  
A<sub>f</sub>: Full flow area in circular section,  
B : Water surface width,  
b : Width of rectangular section,  
C : Runoff coefficient,  
d<sub>g</sub>: Depth in a gutter for peak flow,  
d<sub>s</sub>: Circular sewer diameter,  
g : Gravitational acceleration,  
I : Rainfall intensity,  
I<sub>s</sub>: Design storm intensity,  
K<sub>1</sub>, K<sub>2</sub>: Conversion factors,  
k<sub>1</sub>, k<sub>2</sub>: Coefficients,  
L : Overland flow length of a basin,  
L<sub>o</sub>: Length of subcatchment of an inlet,  
L<sub>g</sub>: Gutter length,  
L<sub>s</sub>: Sewer length,  
n : Manning roughness factor,  
n<sub>g</sub>: Manning roughness factor for gutters,  
n<sub>s</sub>: Manning roughness factor for circular sections,  
n<sub>r</sub>: Manning roughness factor for rectangular sections,  
n<sub>f</sub>: Manning roughness factor for full flow in  
circular sections,  
Q : Flow rate,  
Q<sub>i</sub>: Inlet flow rate,  
Q<sub>j</sub>: Incoming sewer flow rate,  
Q<sub>s</sub>: Sewer flow rate,

NOMENCLATURE (continued)

- $Q_u$ : Sewer upstream flow rate,  
 $Q_G$ : Gutter flow rate,  
 $Q_{ip}$ : Gutter peak flow rate,  
 $Q_p$ : Sewer peak flow rate,  
 $Q_c$ : Carry-over flow rate,  
 $Q_1$ : Inflow rate,  
 $Q_o$ : Outflow rate,  
 $q, q_1$ : Lateral inflow rates,  
 $R$ : Hydraulic radius,  
 $R_f$ : Hydraulic radius for full flow in circular section,  
 $R_g$ : Hydraulic radius for peak gutter flow,  
 $S$ : Average slope of basin, also channel bed slope in Eqs. 3.11 and 3.12,  
 $S_f$ : Friction slope, also full flow slope in Eqs. 3.11 and 3.12,  
 $S_o$ : Bed slope of a channel,  
 $S_s$ : Sewer slope,  
 $S_g$ : Longitudinal gutter slope,  
 $t$ : Time,  
 $t_c$ : Time of concentration,  
 $t_g$ : Gutter flow time,  
 $t_d$ : Storm duration,  
 $t_f$ : Lag time,  
 $t_i$ : Inlet time,  
 $U_1$ : Lateral inflow velocity,  
 $V$ : Flow velocity,

## NOMENCLATURE (concluded)

- $V_f$ : Full flow velocity,  
 $V_p$ : Peak flow velocity,  
 $x$ : Distance,  
 $y$ : Flow depth, also height of rectangular section in Eq. 3.22,  
 $z$ : Street crown slope,  
 $\alpha$ : Percentage of impervious areas,  
 $\theta$ : Angle of channel bed, also central angle of water surface in Eqs. 3.9 and 3.10,  
 $\phi$ : Abstraction index.

## 1. INTRODUCTION

Urban storm drainage implies the collection of storm runoff and conveying it to the nearest point of disposal. An adequate and properly functioning storm water collection system is one of the vital facilities in preserving and improving the urban environment. In newly developing urban areas the first need is certainly a sanitary sewer system as the storm water can be dealt with to a certain extent by the aid of street gutters and the natural water courses. As the city grows, however the underground conveyance of storm water runoff will be necessary. In fact, attempts to provide the greater safety of sewerage, and freedom from nuisance have caused separate storm water collection systems to be adopted wherever finances permit even in small towns of many developed countries. Quite a few recent sewerage project reports among which are those prepared for Ankara (Camp-Harris-Mesara, 1969) and Batıkent (Orta Doğu Teknik Üniversitesi, 1979) recommend the construction of separate storm water collection systems also in the Turkish cities.

The importance of storm water collection systems is usually ignored in the public, since the storm sewers which constitute the main part of the system are buried under the ground and are invisible. However, the investments required for the construction and the maintenance of storm water collection systems are of significant magnitudes. Hence, in order to secure a well functioning storm water collection system, a design engineer must make the best use of the upto date technological tools.

The analysis aspect of the urban storm water collection systems has caught considerable attentions during the last decade. A review and comparisons of a number of rainfall-runoff simulation models have been given by Chow and Yen (1976). Concerning the design of urban drainage systems on the other hand, a limited number of studies are available

in the literature. Yet, these few studies cover a broad spectrum of sophistication varying from very simple models based on rational method (ASCE and WPCF, 1969) to rather sophisticated ones based on the solution of the St. Venant equations (Sevük, 1973). However, as pointed out by Chow (1978), the selection of the most "suitable" model for the field conditions is very difficult since the most suitable does not necessarily mean the most sophisticated. Indeed, there still is much need for research in the design aspect of the stormwater drainage problems in attempts of developing suitable models. Accordingly, the objectives of the present study are:

i. To develop a suitable mathematical model and a computer program for the design of stormwater collection systems.

ii. To illustrate the use of the model through its application to a real world design problem.

iii. To provide a User's Guide for the computer program of the model for future users.

The mathematical model developed is not the most sophisticated one possible. However, it aims to satisfy the basic principles of hydraulics within the limitations of not being inmanagable for practising engineers. The design of both the surface and the subsurface elements of a stormwater collection system is considered. A unique feature of the model makes it possible to group the elements of a system in two different classes according to their importance and accomplish their design by using design storms of two different return periods.

## 2. THEORETICAL BACKGROUND AND RELATED PAST RESEARCH

A stormwater collection system consists of basically street gutters, inlets, sewers, manholes, and main collectors as shown schematically in Fig. 2.1. Street gutters usually constructed on both sides of the street collect stormwater from surfaces such as sidewalks, building roofs, front yards, and driveways and direct it to the inlets. Through the inlets, stormwater is delivered to the subsurface system consisting of stormsewers, collectors and manholes. A storm sewer is a pipe or a conduit of any shape which is intended to carry stormwater or other types of surface runoff reaching the subsurface system. Domestic and industrial wastes are not included in the sewer flow. A collector or main trunk is the principal sewer into which a number of branch sewers discharge. Manholes are structures that provide joining of the sewers as well as convenient access to sewers with the least hydraulic interference for observation and maintenance.

In addition to the basic elements of gutters, inlets, sewers, collectors and manholes; a stormwater collection system may include some special structures like catch basins, siphons and disposal structures. These structures are discussed in detail elsewhere (ASCE and WPCF, 1969) and will not be covered in the present study since they are needed only under special conditions.

### 2.1. Hydraulics of Stormwater Collection Systems

Various types of flows occur in a stormwater collection system. From hydraulics viewpoint these flows can be classified according to their nature into the groups of

- i. overland flow,
- ii. gutter flow,
- iii. flow in sewers and collectors.

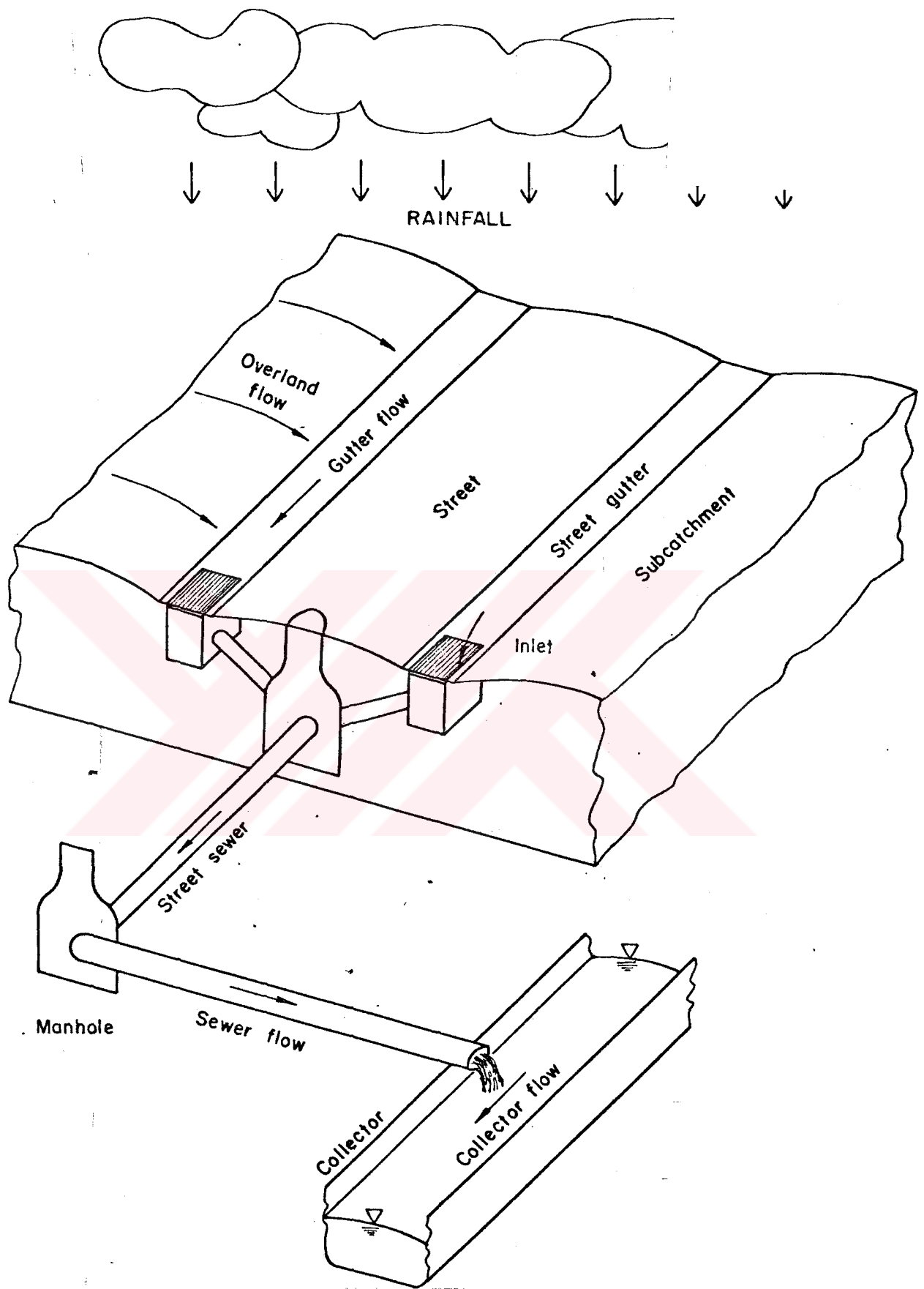


Fig. 2.1 Schematic Representation of a Stormwater Collection System



These flow components are shown in Fig. 2.1. All these components are of unsteady and nonuniform flow type, and they are subject to backwater effects from both ends. They can mathematically be expressed by a set of nonlinear partial differential equations attributed to St. Venant (Chow, 1959). Solutions of such equations can possibly be obtained by numerical techniques, but require a considerable amount of computation time. Therefore certain simplified approaches are inevitable in mathematical models developed for use in the practising engineering.

### 2.1.1. Overland Flow

The movement of rainwater from the point it drops on the earth to a gutter can be represented by an overland flow. This component includes flow over building roofs, gardens, and pedestrian ways. Being a special type of spatially varied unsteady shallow water flow, the overland runoff can be represented by the St. Venant equations (Chow, 1959; Chow and Yen, 1976). For overland flow, St. Venant's continuity and momentum equations can respectively be expressed as

$$\frac{\partial y}{\partial t} + y \frac{\partial V}{\partial x} + V \frac{\partial y}{\partial x} = q \quad (2.1)$$

$$y \frac{\partial V}{\partial t} + yV \frac{\partial V}{\partial x} + gy \cdot \text{Cos}\theta \frac{\partial y}{\partial x} = gy(S_o - S_f) + q(U_1 - V) \quad (2.2)$$

in which  $x$  is the direction of the flow measured along the bed,  $t$  is time,  $V$  is the cross-sectional average flow velocity,  $y$  is the flow depth,  $\theta$  is the angle between the channel bed and the horizontal,  $S_o = \text{Sin}\theta$  is the bed slope,  $S_f$  is the friction slope,  $g$  is the gravitational acceleration,  $q$  is the lateral inflow which is defined as the rate of rainfall reaching the ground minus the rate of infiltration, and  $U_1$  is the velocity of lateral inflow in the direction of  $x$ .

Analytical solutions can not be obtained to the St. Venant equations due to the nonlinear nature of these expressions. A number of numerical schemes have been proposed in the past to solve these equations by using high speed digital computers (Baltzer and Lai, 1968; Amein and Fang, 1969). However, these solutions are cumbersome. Also the boundary conditions for these equations can not be truly and accurately defined in the field conditions. Hence in mathematical modeling of urban storm drainage, overland flow component is determined by simplified approaches rather than attempting to solve the St. Venant equations.

In the practice, peak flow rate of the overland runoff from an urban basin is computed by simple formulas relating the storm intensity and the basin characteristics. Most of such expressions are of empirical nature. Summarized in Table 2.1 are the rainfall-runoff formulas commonly used in urban storm drainage analysis. In this table  $A$  is the basin area in ha,  $I$  is the rainfall intensity in mm/hr, and  $S$  is the average slope of the basin; and  $C$  is a coefficient related to basin characteristics. Among the formulas in the table, Rational formula is the most popular one; and its runoff coefficient  $C$  can be found elsewhere (ASCE and WPCF, 1969).

The expressions of the types given in Table 2.1 are generally based on the assumption that the peak flow rate due to a uniform rainfall occurs when a raindrop from the most remote point in the basin reaches the gutter. The time elapsed from the beginning of the rainfall to occurrence of peak discharge is called the time of concentration of the basin,  $t_c$ . Hence, the intensity  $I$  to be adopted in the expressions given in Table 2.1 should correspond to a rainfall duration of  $t_c$ . The relationship between the intensity and duration depends also on the frequency of the rainfall. These relationships can be exemplified by the family of intensity-duration-frequency curves in Fig. 2.2.

Table 2.1. Some Rainfall-Runoff Formulas for Small  
Drainage Basins (Chow, 1962)

Name	Peak Flow Rate ( m <sup>3</sup> / s)
Adams	$0.00723C \cdot A \cdot I \sqrt[12]{\frac{S}{AI^2}}$
Burkli-Ziegler	$0.06236C \cdot A \cdot I \sqrt[4]{\frac{S}{A}}$
Chamier	$0.011C \cdot A^{0.75} \cdot I$
Hawksley	$0.02778C \cdot A \cdot I \sqrt[4]{\frac{S}{A \cdot I}}$
McMath	$0.00917C \cdot A \cdot I \sqrt[5]{\frac{S}{A}}$
Rational	$0.00278C \cdot I \cdot A$

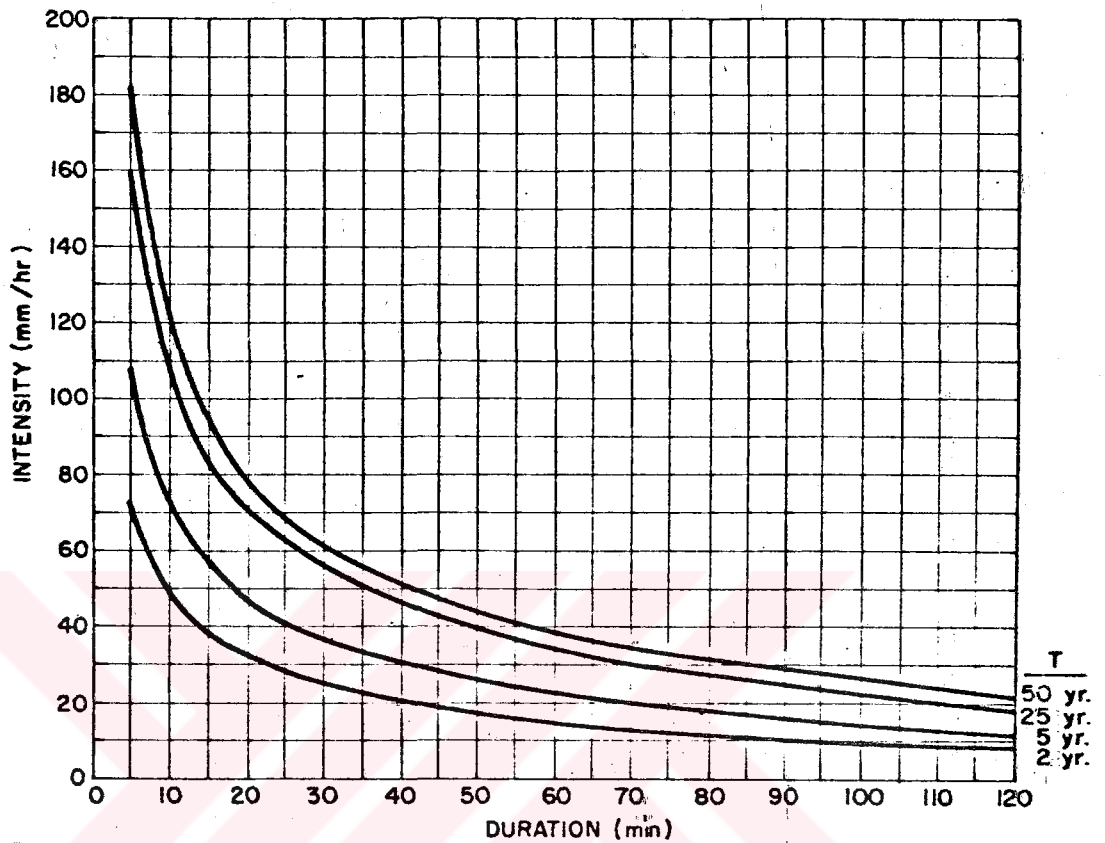


Fig. 2.2. Rainfall Intensity-Duration-Frequency Curves for Ankara

Several formulas proposed for estimating the time of concentration are listed in Table 2.2. In this table  $k_1$  and  $k_2$  are coefficients representing flow resistance,  $n$  is the Manning roughness factor,  $L$  is the overland flow length in m,  $\alpha$  is the percentage of impervious areas,  $I$  is the intensity in mm/hr, and  $S$  is the average slope of the basin.

Table 2.2. Selected Time of Concentration Formulas for Overland Flow (Yen, 1978)

Name	Time of Concentration (min)
Izzard	$526.44(2.754 \times 10^{-5} I^{1/3} \frac{k_1}{I^{2/3}}) (\frac{L}{C^2 S})^{1/3}$
Kerby	$1.446 (\frac{k_2 L}{S^{1/2}})^{0.476}$
Kinematic-wave	$\frac{6.92}{I^{0.4}} (\frac{n^2 L^2}{S})^{0.3}$
Shake et.al.	$\frac{0.670 L^{0.24}}{S^{0.16} \alpha^{0.26}}$

### 2.1.2. Gutter Flow

Runoff in a street gutter occurs in the form of a spatially varied, unsteady open channel flow. As pointed out by Akan and Yen (1980) gutter flow can be represented by St. Venant equations expressed as

$$\frac{\partial A}{\partial t} + \frac{\partial Q}{\partial x} = q_1 \quad (2.3)$$

$$\frac{\partial V}{\partial t} + V \frac{\partial V}{\partial x} + g \frac{\partial y}{\partial x} = g(S_o - S_f) - \frac{V q_1}{A} \quad (2.4)$$

in which  $Q$  is the flow rate,  $t$  is time,  $x$  is the distance along the gutter,  $y$  is the average depth of flow measured normal to  $x$ ,  $V$  is the average velocity of flow,  $q_1$  is the lateral inflow rate from the overland runoff per unit length of the gutter.

As in the case of overland flow component, the solution of the St. Venant equations for gutter flow is costly

and impractical. Hence, simplified approaches are necessary also for gutter flow.

A number of researchers including Huber et. al.(1975), and Chow and Yen (1976) represent the gutter flow by using the variations of the kinematic-wave approximations. The main assumption of the kinematic-wave method is that the friction slope  $S_f$  can be set equal to the bottom slope of an open channel. Hence Eq. 2.4 is simplified to

$$S_o = S_f \quad (2.5)$$

where  $S_f$  is computed by a steady flow friction equation like Manning formula written in metric units as

$$Q = \frac{1}{n} A R^{2/3} S_f^{1/2} \quad (2.6)$$

in which  $Q$  is the flow rate,  $n$  is the Manning roughness factor,  $A$  is the cross-sectional area of the flow,  $R$  is the hydraulic radius, and  $S_o$  is the bottom slope of the gutter. Numerical simultaneous solutions of Eqs. 2.3, 2.5 and 2.6 constitute the gutter flow computations based on a kinematic-wave approach. Further simplifications of gutter flow calculations can be suggested by assuming the flow is steady and uniform with a flow rate equal to the peak surface runoff discharge from the contributing basin (Metcalf and Eddy, 1974). In such an oversimplified approach, Eqs. 2.5 and 2.6 are adopted for gutter flow computations.

### 2.1.3. Flow in Sewers and Collectors

The propagation of stormwater in sewers and collectors can also be described mathematically by the St. Venant equations (Sevük, 1973) as

$$B \frac{\partial y}{\partial t} + BV \frac{\partial y}{\partial x} + A \frac{\partial V}{\partial x} = 0 \quad (2.7)$$

$$\frac{\partial V}{\partial t} + V \frac{\partial V}{\partial x} = gS_o - g \frac{\partial y}{\partial x} - gS_f \quad (2.8)$$

in which  $A, B$  and  $y$  are respectively the cross-sectional area, water surface width, and depth of flow in sewers,  $V$  is the cross-sectional mean velocity,  $S_o$  and  $S_f$  are respectively the sewer or collector bottom and energy grade line slopes,  $x$  is the distance along the sewer, and  $t$  denotes time. As mentioned in Sections 2.1.1 and 2.1.2, analytical solution of Eqs. 2.7 and 2.8 is not possible and the solution of these equations by numerical techniques is cumbersome and costly for urban storm drainage conditions. Therefore, simplified approaches among which is the kinematic-wave method have been devised in the past for flow routing in storm sewers (Huber et. al., 1975; Yen and Sevük, 1975). The application of the kinematic-wave to sewer flow is essentially the same as for gutter flow.

Another simplified approach for sewer flow routing is the hydrograph time-lag method. In this approach an upstream inflow hydrograph of a sewer is carried to the downstream end without any distortion in its shape. However, the hydrograph is shifted by a lag time estimated from the length of the sewer and a characteristic flow velocity.

## 2.2. Review of Major Urban Storm Drainage Models

A review of the major existing models for the analysis and design of urban storm drainage system are given here in view of the basic hydraulic considerations discussed in the preceding sections. Such a review is especially useful for evaluating the mathematical model developed in the present study.

### 2.2.1. Rational Method

Rational method is the most popular approach for practising engineers for sewer system design due to its simplicity. The method is based on the rational formula given in Table 2.1. On the other hand, in application of

the rational formula to sewer design, the time of concentration is taken as the summation of the inlet time and the sewer flow time. The sewer system is designed starting from the most upstream sewers and proceeding sequentially towards downstream. The rational method has no theoretical justification.

#### 2.2.2. Chicago Hydrograph Method

The overland flow component in the Chicago Hydrograph Method is calculated by using Izzard's synthetic hydrograph approach (Tholin and Keifer, 1960). Gutter and sewer flows are determined from a linearized version of the kinematic-wave approximation. Sewers are designed in a sequential manner starting from the upstream ones. The peak inflow rate for each sewer is adopted as the design discharge.

#### 2.2.3. Transport Road Research Laboratory (TRRL) Method

The inlet hydrographs are determined by algebraically summing the contributions from the subcatchment of impervious surfaces which have equal flow times to the point of inlet. Contributions from pervious surfaces are neglected. Inlet hydrographs are routed in the sewer system by using a hydrograph time-lag method in corporation with a storage routing scheme. The downstream hydrograph of each sewer is first approximately determined by a time-lag approach, then it is modified by using a storage routing scheme (Terstriap and Stall, 1969). Again the peak inflow rate of each sewer is adopted as the design discharge.

#### 2.2.4. Illinois Urban Drainage Area Simulator (ILLUDAS)

ILLUDAS is a modification of the TRRL method essentially to account for the surface runoff from pervious areas (Terstriap and Stall, 1974). Also the sewer routing scheme is somehow improved by using a scheme which can be classified as a linearized kinematic-wave method.



### 2.2.5. EPA Stormwater Management Model (SWMM)

SWMM is a relatively comprehensive model considering both quantity and quality aspects of stormwater runoff. It utilizes linear kinematic-wave approximations for overland and gutter flows, and a modified nonlinear kinematic-wave approach for sewer flow computations. The modification of the nonlinear scheme is provided for the purpose of accounting for the backwater effects to a certain extent in the sewer system.

### 2.2.6. Illinois Urban Storm Runoff (IUSR) Method

IUSR employs a nonlinear kinematic-wave scheme for flow routing in the overland flow surfaces and gutters. Inlet hydrographs are computed considering the interception capacities of the inlets which may behave either as weirs or orifices depending on the gutter flow conditions. Carry-overs from inlets are allowed (Chow and Yen, 1976). A dynamic-wave flow routing scheme is employed for flow in the sewers. Backwater effects from the joining sewers and the manholes on sewer flow are considered.

### 3. DESCRIPTION OF PROPOSED MATHEMATICAL MODEL

The proposed mathematical model differs from most of the existing models in several aspects. The highlights of the model can be summarized as follows:

i. The required number and the locations of the gutter inlets in the drainage area are determined as part of the model output.

ii. Neither the sewer section sizes nor the slopes are to be specified by the user. The model attempts to select a proper combination of a sewer section size and a slope according to a minimum soil cover and a maximum allowable velocity criterion.

iii. Considering possible flood damages due to a failure of each element, components of a storm drainage system are categorized into two groups. Then those elements in different groups are designed by use of design storms of different return periods.

iv. A hydrograph time-lag method is adopted for flow routing in the gutters, sewers and the collectors. Also an optional simplified kinematic-wave technique is provided for unsteady flow computations in the sewers and the collectors.

#### 3.1. Grouping of the Elements

Since the failure of different elements in a storm drainage system cause different magnitudes of flood damages; from engineering economy viewpoint, these elements need to be designed considering design storms of different return periods. In the proposed model the elements of an urban drainage system are categorized into two groups.

Gutter inlets, street sewers, and manholes constitute the first group; and they are designed for a rain-storm of a small return period like 2 to 5 years. Main

collectors are in the second group and they are designed considering a more severe rainstorm with a return period of 10 to 25 years. Accordingly, the design of a storm drainage system is completed in two stages. Elements of the first group are designed in the first stage; and the main collectors are dimensioned in the second stage. Evidently, the hydraulic response of the first group Elements under a rainstorm more severe than their design -storm need to be simulated in the second stage of the design procedure.

### 3.2. Design of First-Group Elements

Gutter inlets, street sewers, and manholes are included in the first group. These elements are designed according to a design storm with a return period of 2 to 5 years. Manholes are selected among the standard types with sizes depending upon the section sizes of the incoming and outgoing sewers. Hence no means are provided in the model to compute the manhole dimensions.

#### 3.2.1. Gutter Inlets

Gutter inlets are first placed at the corners of each block. The number and the locations of additional gutter inlets required are then determined such that no carry-over from an inlet is allowed under the conditions of the design storm. This is accomplished by providing an inlet wherever the peak gutter discharge is likely to exceed a specified magnitude. Alternatively, the spacings of the inlets may be controlled such that the flow depth in the gutter will not exceed a specified maximum allowable depth.

##### 3.2.1.1. Inlet Hydrographs

The drainage area is divided into a number of sub-catchments, each flowing into a gutter inlet existing in the drainage system. Since no carry-over is allowed from an inlet under the design-storm conditions, the entire

rainfall excess from a subcatchment is intercepted by the associated gutter inlet. As suggested by Yen and Cheng (1980) the inlet hydrographs are assumed to be triangular or trapezoidal in shape as shown in Fig. 3.1 depending upon the relative magnitudes of the inlet time  $t_i$  and the duration of the design storm  $t_d$ . If the storm duration  $t_d$  is equal or greater than inlet time  $t_i$ , the peak discharge is equal to

$$Q_{ip} = A_i (I_s - \phi) \quad (3.1)$$

in which  $Q_{ip}$  is the peak inflow rate of the inlet,  $A_i$  is the subcatchment area of the inlet,  $I_s$  is the intensity of design storm, and  $\phi$  is the abstraction index. For the inlets which have inlet times greater than the rainfall duration, the peak flow rate of the inlet hydrograph is calculated as

$$Q_{ip} = \frac{t_d}{t_i} A_i (I_s - \phi) \quad (3.2)$$

in which the terms are as defined previously. An inspection of Fig. 3.1 together with Eqs. 3.1 and 3.2 reveals that the volumes of the inlet hydrographs are equal to the net effective rainfall volume occurring over the corresponding subcatchment.

The abstraction index  $\phi$  in Eqs. 3.1 and 3.2 consist of the losses mainly due to the infiltration into the soil and depressions storage. As pointed out by ASCE and WPCF (1969) the infiltration capacity of various types of bare soils after one hour of continuous rainfall can be estimated as 12.5-25.0 mm/hr for sandy, open-structured soils; 2.5-12.5 mm/hr for loam; and 0.2-2.0 mm/hr for clay, close-structured soils. The infiltration capacity is 3-7.5 times greater for surfaces covered with grass. For detention losses 0.25 cm loss throughout the rainfall duration must be taken into account. Evidently the soil conditions such as saturation of the soil prior to

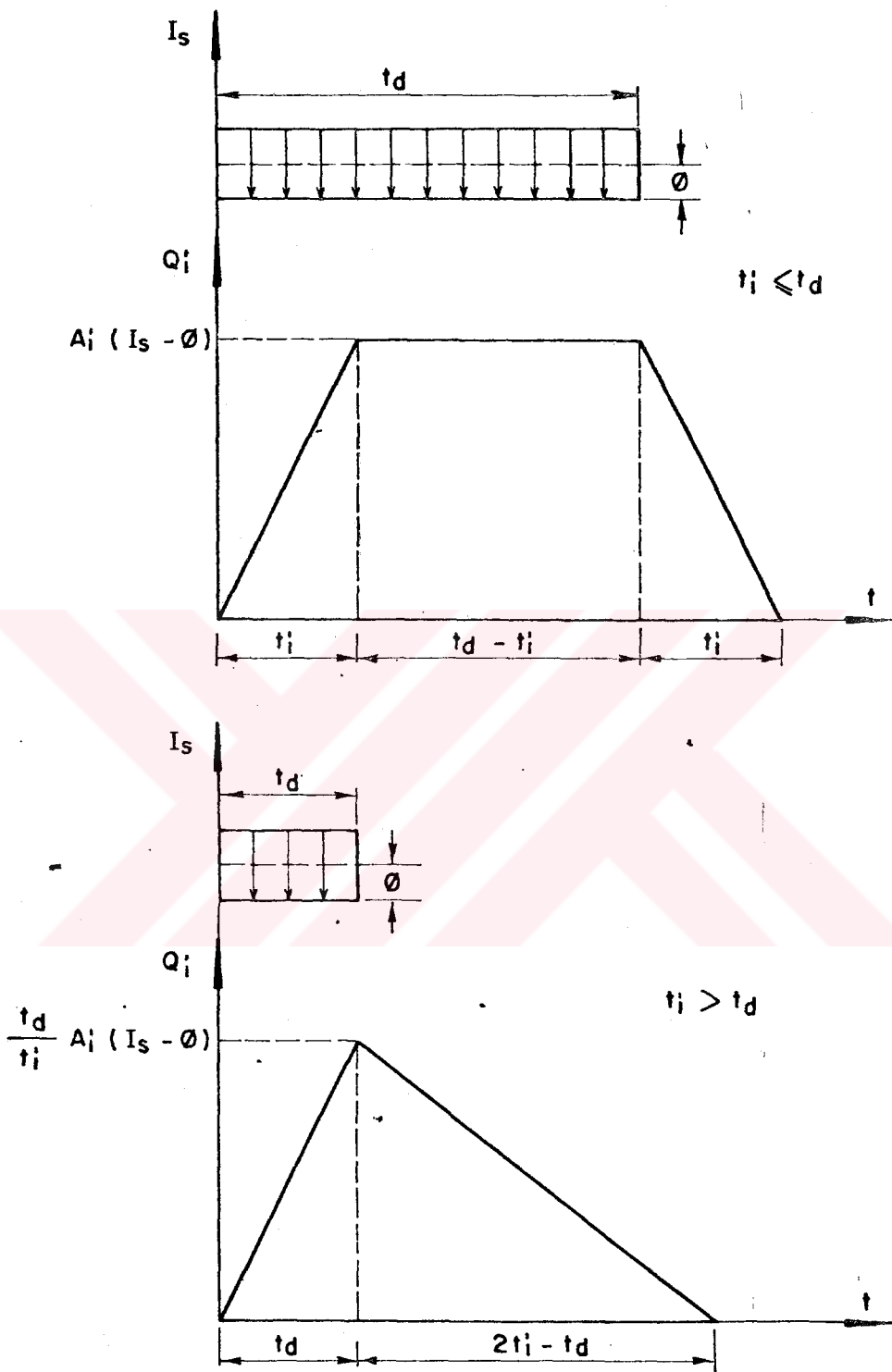


Fig. 3.1. Inlet Hydrographs

the rainfall greatly affect the infiltration capacity. In design, the selection of lower limits will provide safety.

The inlet time  $t_i$  is equal to the summation of the time of concentration  $t_c$  for the subcatchment and the gutter flow time  $t_g$ . The time of concentration is computed by using the kinematic-wave formula (Yen, 1978).

$$t_c = \frac{K_1}{I_s^{0.4}} \left[ \frac{n^2 L_o^2}{S_s} \right]^{0.3} \quad (3.3)$$

in which  $L_o$  is the subcatchment flow length,  $S_s$  is the the average slope of the subcatchment,  $n$  is Manning roughness factor, and  $K_1$  is a conversion factor. Suggested values of  $n$  for different types of land use are given in Appendix A. The conversion factor  $K_1$  is 0.93 for the British unit system and it becomes 6.92 when  $t_c$  is in min,  $I_s$  is in mm/hr, and  $L_o$  is in m. The gutter flow time  $t_g$  is computed from Manning formula as

$$t_g = K_2 L_g n_g / (R_g^{2/3} \cdot S_g^{1/2}) \quad (3.4)$$

in which  $L_g$  is the length of the gutter,  $n_g$  is the Manning roughness factor,  $S_g$  is the longitudinal gutter slope and  $R_g$  is the hydraulic radius corresponding to the peak flow rate. The conversion factor  $K_2$  is 1/60 when  $t_g$  is in min; and  $R_g$  and  $L_g$  are both in m.

### 3.2.1.2. Additional Inlets

The peak flow rate of an inlet hydrograph is checked against the allowable maximum gutter discharge in order not to permit any carry-over from an inlet. Allowable gutter discharge corresponds to the interception capacity of a standard-type inlet, and it is about 50 lt/s (İller Bankası, 1971).

Exceedance of the maximum allowable gutter discharge by a peak inlet flow rate implies a need for additional inlets along the gutter. These additional inlets are placed with equal spacing; the number of which is calculated such as the maximum gutter discharge criterion is not violated. The calculation of the number of the additional inlets requires a trial-and-error procedure.

Optionally the mathematical model permits a maximum allowable gutter flow depth to be specified instead of an allowable discharge for controlling the inlet spacing. The maximum allowable gutter flow depth may be limited by the curb height or it can be selected such that the top width of the gutter flow will not exceed the width of the inlet. The gutter flow depth corresponding to the peak discharge is computed by using the Manning formula written in metric units as

$$d_g = 1.54 \left[ \frac{Q_{ip} \cdot n_g}{z \cdot S_g^{1/2}} \right]^{3/8} \quad (3.5)$$

in which  $d_g$  is the flow depth in the gutter assumed triangular in cross section,  $z$  is the reciprocal of street crown slope,  $S_g$  is the longitudinal slope of the gutter, and  $n_g$  is the Manning roughness factor of the gutter. If  $d_g$  thus computed exceeds the specified allowable depth, then additional inlets are placed with equal spacings along the gutter. The number of these additional inlets are determined such that the allowable depth criterion is satisfied.

Main assumption of placing additional inlets at equal intervals is that the basin area, and the characteristics of the basin is uniformly distributed along the gutter; and the slope of the gutter is constant. Where additional inlets are placed, the inlet hydrographs are recomputed following the procedure given in Section 3.2.1.1.

### 3.2.2. Design of Street Sewers

Street sewers are designed sequentially starting from the most upstream ones and proceeding in the downstream direction. The size of a sewer is computed such that a maximum allowable velocity will not be exceeded at the peak discharge of the upstream inflow hydrograph of the sewer. The upstream inflow for a sewer consists of the outflows from the further upstream sewers, and the surface runoff contributing directly to the manhole attached to the upstream end of the sewer. The direct surface runoff input is expressed by the corresponding inlet hydrographs. Also, a flow routing scheme is provided to find the discharge hydrographs at the downstream ends of the sewers. This information is necessary to carry out the design procedure to further downstream sewers.

#### 3.2.2.1. Selection of Sewer Size and Slope

Street sewers are designed starting from the most upstream pipes and progressing in sequence one by one towards downstream. The inflow hydrograph of a sewer is computed by using the formula

$$Q_u = \sum Q_i + \sum Q_j \quad (3.6)$$

in which  $Q_u$  is the upstream inflow rate for the sewer,  $\sum Q_i$  is the summation of the inlet flow rates discharging directly into the manhole connected to the upstream end of the sewer, and  $\sum Q_j$  is the sum of the discharges from the upstream sewers joining the same manhole. Evidently  $\sum Q_j$  is zero for the sewers located at upstream extremities of the system. The peak flow rate  $Q_p$  of the upstream inflow hydrograph is selected to be the design discharge. The required sewer size is determined from the Manning formula according to a specified section type. If circular sections are desired, the required sewer diameter  $d_s$  is calculated in m as

$$d_s = 1.548(Q_p n_s / \sqrt{S_s})^{0.375} \quad (3.7)$$



in which  $Q_p$  is the peak inflow rate in  $m^3/s$ ,  $n_s$  is the Manning roughness factor for circular sewer, and  $S_s$  is the sewer slope. The next standard sewer size larger than  $d_s$  is selected. If rectangular sections are desired, the required section type is determined by calculating the conveyance factor

$$A-R^{2/3} = \frac{Q_p n_r}{\sqrt{S_s}} \quad (3.8)$$

in which  $n_r$  is the Manning roughness factor for rectangular sections, and the other terms are as defined previously. Standard rectangular section with a greater conveyance factor is chosen for that peak discharge at the adopted sewer slope.

In order to minimize the excavation work, first the associated street slope is adopted and employed in Eqs. 3.7 and 3.8 as the sewer slope. Then the design flow velocity is calculated by using the selected sewer slope and the size. If the computed velocity is smaller than the maximum allowable velocity, the design is accepted. In cases the calculated velocity exceeds the maximum allowable velocity, depending upon the choice of the user, either the sewer size is increased or the sewer slope is decreased to values at which the maximum velocity criterion is satisfied. If a change in sewer slope is preferred, chute structures are added to the system for the purpose of satisfying the minimum soil cover requirement. The heights of the chute structures are also computed in the model. The user is allowed to specify the number of the larger standard size sections to be tried as an alternative to the chute structures for satisfying the maximum allowable velocity criterion.

Since sewers are designed to flow partially filled, the design flow velocity to be checked against the maximum allowable velocity is computed for partially filled flow conditions. In circular sections, due to the geometry, no explicit expressions are available to compute the flow velocity. The relationships between the cross-sectional

properties of partially filled circular sewers are expressed in terms of the full flow parameters as

$$\frac{A}{A_f} = \frac{\theta}{360} - \frac{\sin\theta}{2\pi} \quad (3.9)$$

$$\frac{R}{R_f} = 1 - \frac{360\sin\theta}{2\pi\theta} \quad (3.10)$$

$$\frac{V}{V_f} = \frac{n_f}{n} \cdot \left( \frac{R}{R_f} \right)^{2/3} \cdot \left( \frac{S}{S_f} \right)^{1/2} \quad (3.11)$$

$$\frac{Q}{Q_f} = \frac{n_f}{n} \cdot \frac{A}{A_f} \cdot \left( \frac{R}{R_f} \right)^{2/3} \cdot \left( \frac{S}{S_f} \right)^{1/2} \quad (3.12)$$

in which A is the flow area, R is the hydraulic radius, V is the flow velocity, Q is the flow rate, n is the Manning roughness factor, S is the slope of the sewer, and  $\theta$  is the central angle of the surface in degrees. The parameters with subscript f denotes the hydraulic properties for full flow case. These relationships can also be represented graphically as shown in Fig. 3.2 (ASCE and WCPF, 1969). The variation in Manning roughness factor with flow depth is accounted for Eqs. 3.11 and 3.12, and as well as in Fig. 3.2. In the mathematical model the flow velocity is computed by using the relationships given above. Values for Manning roughness factor for full flow conditions are given in Appendix A.

Since the slopes of the sewers in the system vary, Eqs. 3.7 or 3.8 may yield a sewer section size smaller than that of upstream one. However as recommended by ASCE and WCPF (1969), the mathematical model does not allow any reduction in sewer size in the flow direction. In other words, a sewer outgoing from a manhole can not be smaller in size than any one of the incoming sewers.

As the design of a sewer is completed the discharge

hydrograph at its downstream end is calculated by use of a routing scheme.

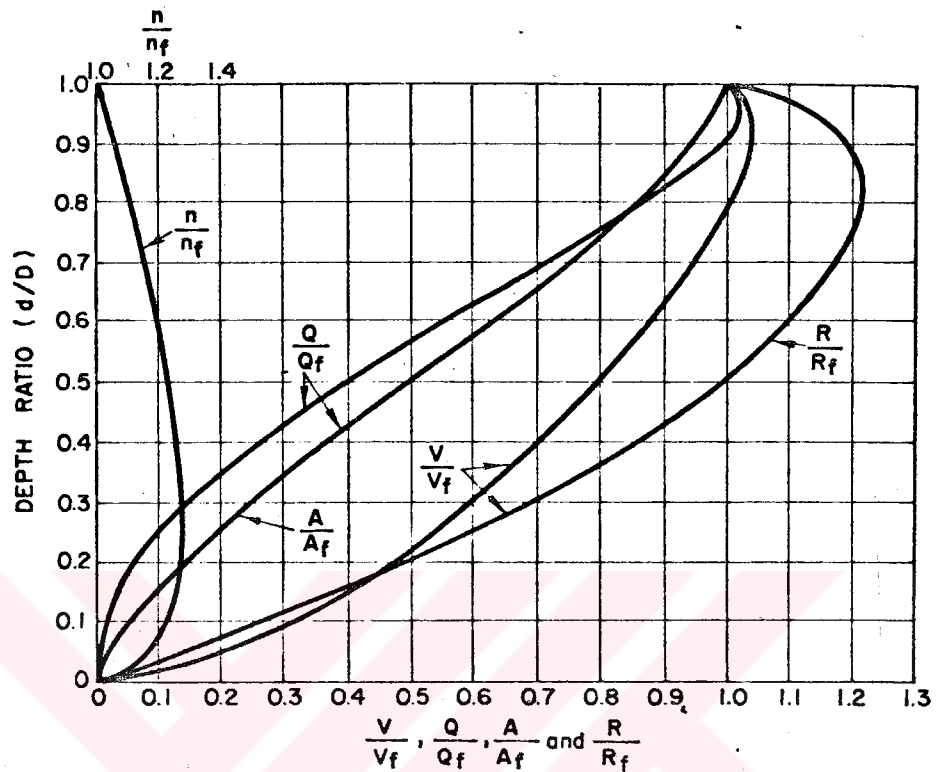


Fig. 3.2. Hydraulic Elements of Partly Filled Circular Sewers (ASCE and WPCF, 1969)

### 3.2.2.2. Sewer Flow Routing

The user of the model is allowed to select one of the two routing schemes devised for determining discharge hydrographs at the downstream ends of the sewers. The first scheme is based on a hydrograph time-lag method, and the second scheme is a simplified version of a kinematic-wave model.

The sewer flow time  $t_f$  required in the hydrograph time-lag scheme is computed by

$$t_f = \frac{L_s}{V_p} \quad (3.13)$$

in which  $L_s$  is the length of the sewer and  $V_p$  is the peak flow velocity. Then, as shown in Fig. 3.3, the upstream inflow hydrograph of a sewer is shifted by  $t_f$  along the time axis to determine the sewer outflow hydrograph.

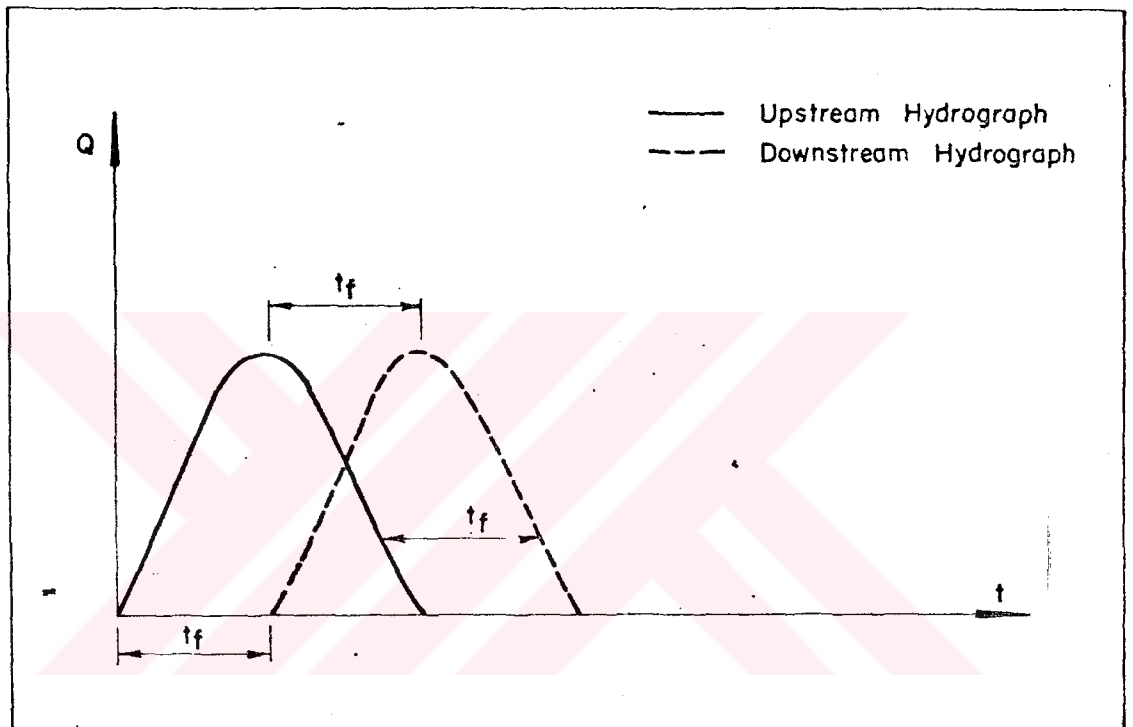


Fig. 3.3. Hydrograph Time - Lag Method for Sewers

The simplified kinematic-wave scheme is based on the continuity equation of unsteady flow and the Manning formula given in Eqs. 2.7 and 2.6 respectively. For a sewer in the system, Eq. 2.7 can be written in finite difference form as

$$\frac{A^{j+1} - A^j}{\Delta t} + \frac{Q_1^{j+\frac{1}{2}} - Q_0^{j+\frac{1}{2}}}{L_s} = 0 \quad (3.14)$$

in which the subscript  $j$  and  $j+1$  represent the time steps of computation,  $A$  is the average flow area in the sewer,  $\Delta t$  is time increment,  $Q_1$  is the inflow rate,  $Q_0$  is the outflow rate, and  $L_s$  is the length of the sewer.

In the routing procedure, the variables at the  $j$  th level of computation are known from the previous time step calculations or from the initial conditions. Also  $Q_1^j$  and  $Q_1^{j+1}$  values are known from sewer inflow hydrograph. The computations are carried to the  $j+1$  st time step as follows:

i. The rate of inflow to the sewer is averaged over a time increment  $\Delta t$  by

$$Q_1^{j+\frac{1}{2}} = \frac{1}{2} (Q_1^j + Q_1^{j+1}) \quad (3.15)$$

ii. The increase in sewer flow area over the half time increment  $\Delta t/2$  is expressed by  $\Delta A'$  and computed approximately as

$$\Delta A' = \frac{\Delta t}{2L_s} (Q_1^{j+\frac{1}{2}} - Q_0^j) \quad (3.16)$$

iii. The average rate of outflow from the sewer  $Q_0^j$  is calculated as a function of  $A^{j+\frac{1}{2}} = A^j + \Delta A'$  in the form of

$$Q_0^{j+\frac{1}{2}} = f(A^{j+\frac{1}{2}}) \quad (3.17)$$

by using the Manning formula together with Eqs. 3.9 to 3.12

iv. The change in the average sewer flow area  $\Delta A$  over the time interval  $\Delta t$  is calculated as

$$\Delta A = \frac{\Delta t}{L_s} (Q_1^{j+\frac{1}{2}} - Q_0^{j+\frac{1}{2}}) \quad (3.18)$$

v. The average sewer flow area at the  $j+1$  st time level is calculated as

$$A^{j+1} = A^j + \Delta A \quad (3.19)$$

vi. The sewer outflow rate at the  $j+1$  st time level is computed in the form of

$$Q_o^{j+1} = f(A^{j+1}) \quad (3.20)$$

by using The Manning formula together with Eqs. 3.9 to 3.12

### 3.3. Design of Second-Group Elements

Design discharges adopted for sizing the first-group elements are exceeded in the second-stage of design in which the collectors are dimensioned considering a more severe rainstorm. Hence under the conditions of the second-stage design storm, part of the storm water floods the streets even though the street sewers may be discharging continuously at their full capacity. This excess storm water which can not enter the sewer system is routed in the gutters towards the nearest collector following a surface drainage pattern specified by the user. A simulation of flow in first group elements is devised to find the design discharges for the second-group elements.

#### 3.3.1. Simulation of Flow in First-Group Elements

Simulation of the first-group elements consists of the routing of flow in the street gutters and the street sewers. The procedure is started from the most upstream gutters and sewers, and carried in a sequential manner towards downstream following the specified drainage pattern.

##### 3.3.1.1. Gutter Flow Routing

Besides the carry-over from an upstream inlet, a gutter receives lateral inflow from the contributing subcatchment. The lateral inflow hydrographs are determined in a similar fashion as in Fig. 3.1 except that the inlet time  $t_i$  is replaced by the time of concentration  $t_c$ . The routing for the gutter flow is accomplished by a hydrograph time-lag approach. In this approach, a gutter is divided into a number of segments as specified by the user. As

illustrated in Fig. 3.4 the upstream inflow hydrograph is first carried down along the most upstream segment of the gutter by a time-lag equal to the flow time calculated from the length of this segment. The flow time is computed for the peak flow rate of the gutter hydrograph as in Eq. 3.4 except the length of the gutter segment is substituted in place of the entire gutter length  $L_g$ . The shifted hydrograph is then algebraically summed up with the lateral inflow of this segment. The resulting hydrograph is routed through the next segment downstream in the same manner and added to the lateral inflow of that segment. The same procedure is repeated until the downstream end of the gutter is reached.

### 3.3.1.2. Flow into Gutter Inlets

Since in the design of second-group elements, the design discharges of the first-group exceeded, surcharge conditions are likely to occur in the system. Under the surcharge conditions only part of the surface runoff is captured by the gutter inlets. The flow interception capacity of a gutter inlet is assumed to be controlled by the full flow discharge capacity,  $Q_f$  of the street sewer downstream as shown in Fig. 3.5. The full capacity  $Q_f$  is computed in  $m^3/s$  from the Manning formula as

$$Q_f = 0.312 d_s^{8/3} S_o^{1/2} / n_s \quad (3.21)$$

for circular sewers, and  $Q_f$  is computed as

$$Q_f = \frac{1}{n_r} \cdot b \cdot y \cdot \left[ \frac{b \cdot y}{b + 2y} \right]^{2/3} \cdot S_o^{1/2} \quad (3.22)$$

for rectangular sewers. In Eqs. 3.21 and 3.22  $d_s$  is the sewer diameter in m,  $S_o$  is the longitudinal street slope,  $b$  and  $y$  are width and height of the rectangular section in m respectively. The use of the street slope  $S_o$  in Eqs. 3.21 and 3.22 is based on the assumption that the hydraulic grade line is approximately parallel to the

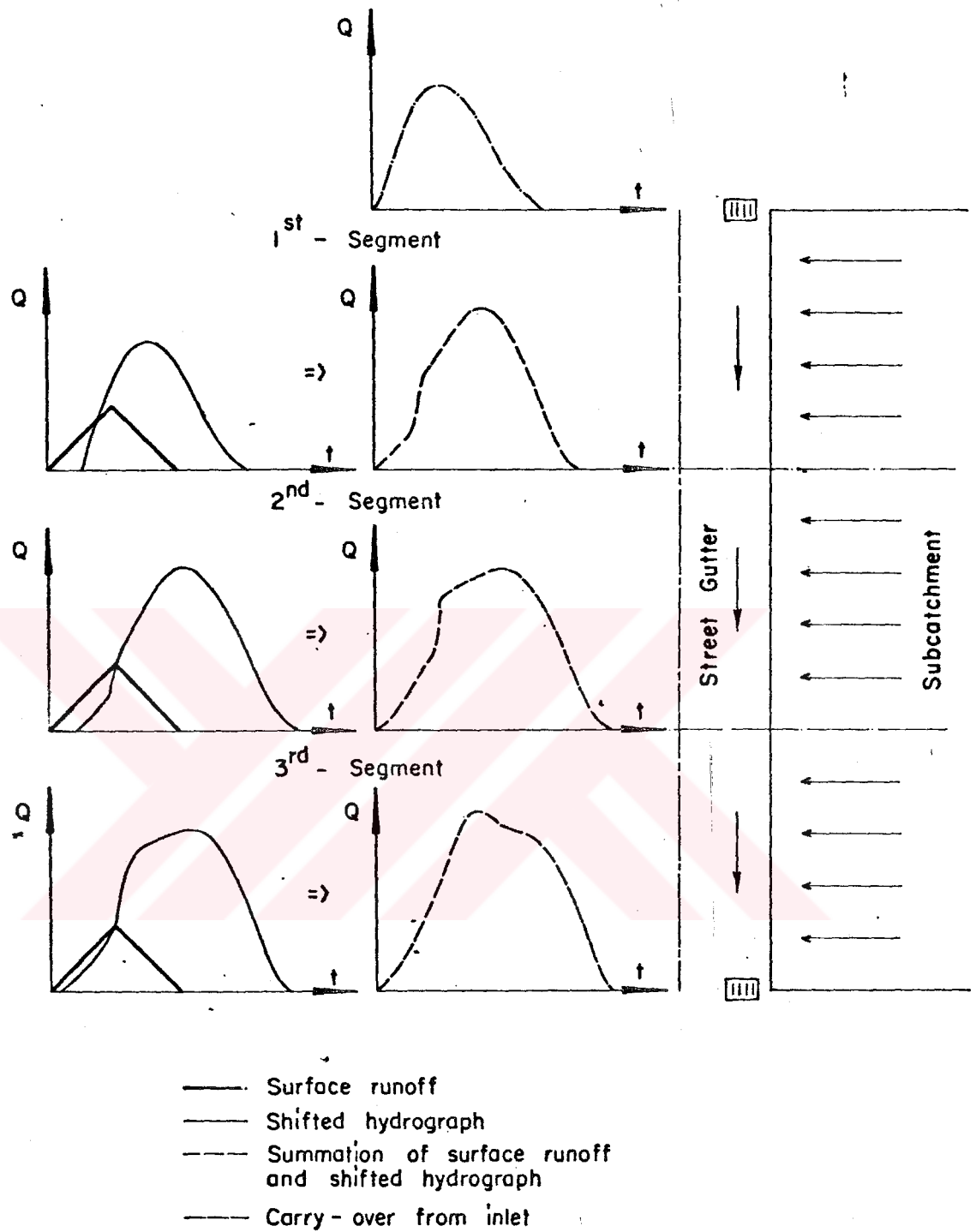


Fig. 3.4. Time - Lag Method for Gutter Flow Routing



street surface under the surcharge conditions.

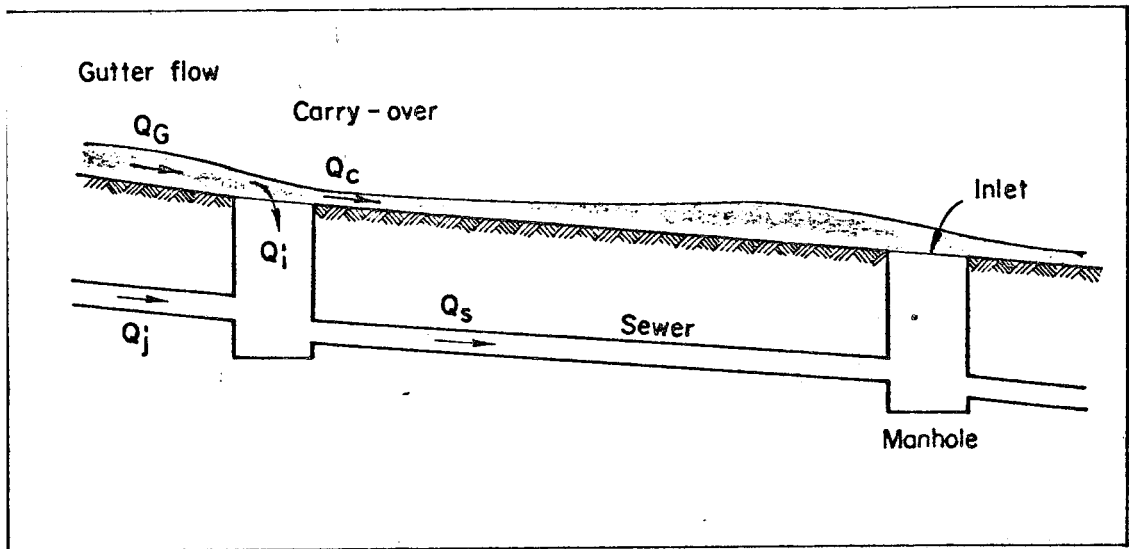


Fig. 3.5 Surcharge Condition

At any time of computation knowing  $Q_G$  and  $\sum Q_j$  computed respectively from upstream gutter and sewer routing schemes and  $Q_f$  determined from Eq. 3.21 or 3.22; the intercepted flow  $Q_i$ , the carry-over  $Q_C$  and the sewer inflow  $Q_s$  are estimated as follows:

i. If  $Q_f \leq Q_G + \sum Q_j$

$$Q_i = Q_f - \sum Q_j \quad (3.23)$$

$$Q_C = Q_G - Q_i \quad (3.24)$$

$$Q_s = Q_f \quad (3.25)$$

ii. If  $Q_f > Q_G + \sum Q_j$

$$Q_i = Q_G \quad (3.26)$$

$$Q_C = 0.0 \quad (3.27)$$

$$Q_s = Q_G + \sum Q_j \quad (3.28)$$

Calculating  $Q_i$ ,  $Q_C$  and  $Q_s$  at different time step computations, the inflow hydrographs for the downstream gutters and the street sewers are determined.

### 3.3.1.3. Sewer Flow Routing

Upstream inflow of a street sewer is computed as described in Section 3.3.1.2. This hydrograph is then routed along the sewer by using one of the routing schemes as discussed in detail in Section 3.2.2.2.

### 3.3.2. Design of Collectors

Storm water reaching the collectors partly through the sewer system and partly over the street surfaces constitute the inflows for these elements. Mathematical model allows the use of additional direct inflow hydrographs to be specified for the collectors which may be contributions from those parts of the drainage basin not included in the simulation.

Collectors are designed starting from the most upstream canals and progressing in sequence towards downstream. The design procedure of the collectors is the same as that of the street sewers as discussed in Section 3.2.2.

### 3.4. Options of model

The major options of the mathematical model can be summarized as follows:

i. Two sewer routing schemes namely a hydrograph time-lag and a simplified kinematic-wave method are provided.

ii. Sewers can be designed circular or rectangular in cross section.

iii. Collectors can be designed circular, rectangular or trapezoidal in cross section

iv. For any street in the drainage area, a pair of sewers on the two sides of the street or a single sewer

at the center can be selected. However, when a single sewer is used, the sewer size is not recomputed where additional inlets are required.

v. Where the maximum flow velocity is exceeded in a sewer or collector laid parallel to the ground surface, the size of the sewer may be increased, or the slope may be decreased with the incorporation of the chute structures. Also the user may desire checking the both alternatives by specifying the number of the larger standard sizes to be tried as a preference over the chute structures.

### 3.5. Computer Program

A computer program in FORTRAN IV language is developed for the mathematical model proposed in this study. It consists of a main program and seven subroutine programmes with 1002 FORTRAN statements. The description, listing, and a user's guide of the computer program is given in Appendix B.

#### 4. APPLICATION OF PROPOSED MODEL

The proposed model is applied to an approximately 29.3 ha basin in the Batıkent Satellite Town near Ankara. The topography and the land use of this area is shown in Fig. 4.1. Also shown in this figure are the drainage pattern and the abstraction indices of the subcatchments as well as the sewer layout and the collectors. The sewers and the collectors are circular in cross section. The design storm adopted for the street sewers has an intensity of 68 mm/hr and a duration of 15 min, and that for collectors has an intensity of 88 mm/hr and a duration of 35 min. The collector receives an upstream inflow from a 7.21 ha basin not shown in Fig. 4.1. This upstream inflow is represented by a hydrograph with a peak discharge of 553 lt/s and a time base of 121 min entering the collector at the flow section marked 77 in Fig. 4.1.

In order to provide a comparison of the two schemes, solutions are obtained by using both the hydrograph time-lag and simplified kinematic-wave routing methods. The major input data and the results are summarized in Table 4.1.

An inspection of Table 4.1 reveals that the sewer design discharges computed are very close and the sewer diameters are identical. On the other hand, the sizes of the collectors computed by the two schemes are different. This is mainly due to the fact that equilibrium (steady state) conditions are reached in the sewers and hence the peak discharges estimated by the two methods are essentially the same. Steady state conditions can be observed from Fig. 4.2 and 4.3 which show the flow hydrographs obtained at sections 15 and 76 in the sewer system. Conversely, in the collectors, steady state is not reached, and hence the attenuation of the peak flow which is accounted for by the simplified kinematic-wave approach but not considered in the time-lag method becomes an important factor. Expectedly the hydrograph peaks are greater

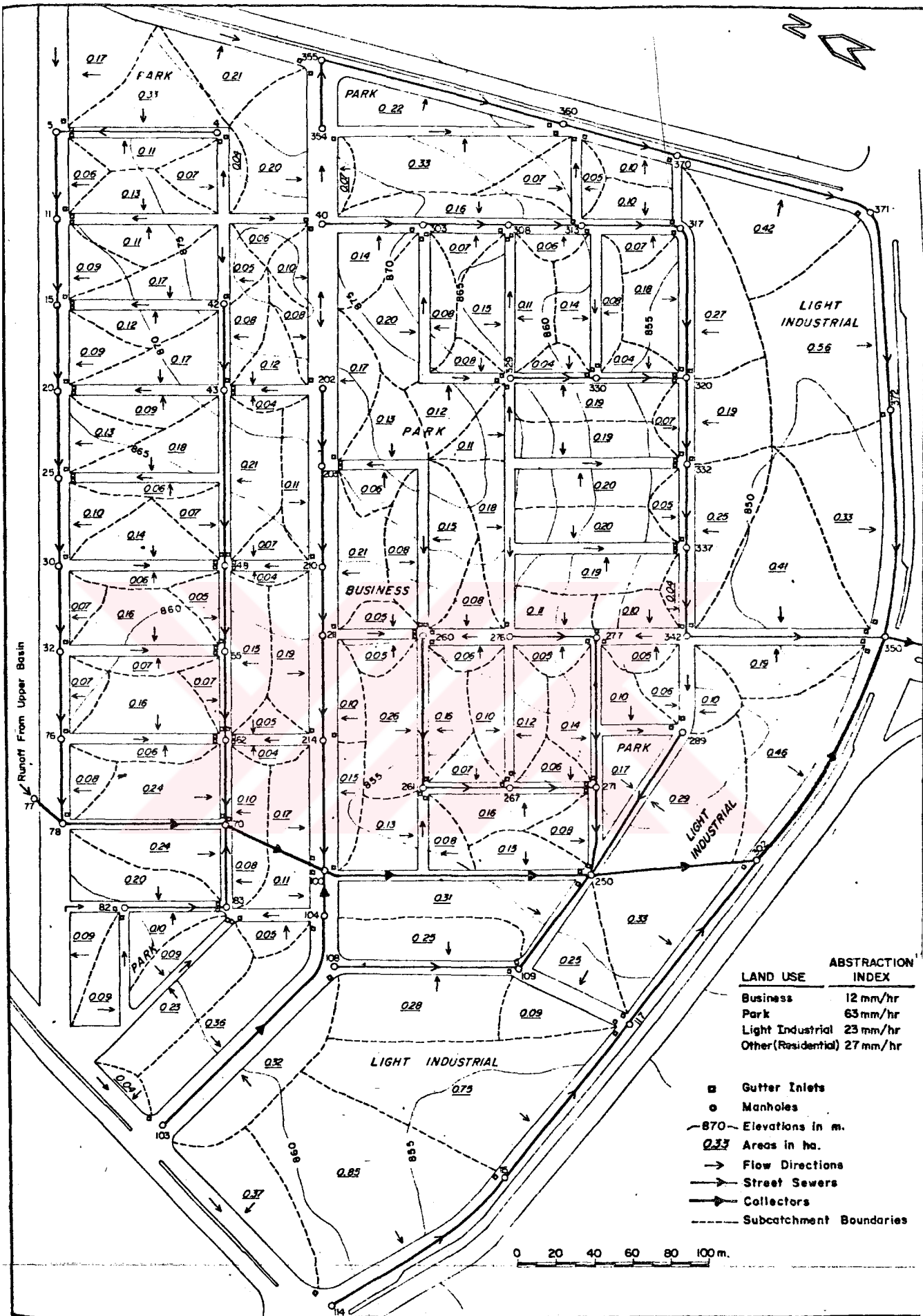


Fig. 4.1. Details of Drainage Basin

Table 4.1. Computed Street Sewer and Collector Discharges and Diameters (to be continued)

From Node	To Node	Drained		Kinematic-wave		Hydrograph time-lag	
		Area ha	Slope %	Discharge lt/s	Diameter mm	Discharge lt/s	Diameter mm
4	5	0.11	8.23	9	200	9	200
5	11	0.72	2.71	28	200	28	200
11	15	1.02	3.40	62	250	62	250
15	20	1.40	3.70	105	300	105	300
20	25	1.75	5.59	145	300	105	300
25	30	2.12	2.41	187	400	187	400
30	32	2.22	1.66	199	400	199	400
42	43	0.05	12.51	6	200	6	200
43	48	0.29	10.66	33	200	33	200
48	55	0.88	5.38	100	250	100	250
55	62	1.16	2.77	132	350	132	350
32	76	2.29	1.52	207	400	206	400
77	78	7.21	8.94	553	500	553	500
76	78	2.36	0.53	215	500	213	500
78	70	9.65	3.84	546	500	808	600
62	70	1.69	1.64	193	400	193	400
82	83	0.18	5.48	21	200	21	200
83	70	0.85	0.26	73	400	73	400
70	100	12.85	1.09	1021	800	1315	1000
103	104	0.04	4.10	5	200	5	200
104	100	0.40	10.14	46	200	46	200
202	203	0.08	6.96	9	200	9	200
203	210	0.44	6.96	23	200	23	200
210	211	0.55	5.46	30	200	30	200
211	214	0.76	8.17	56	200	56	200
214	100	1.05	4.08	89	250	89	250
100	250	14.73	0.29	1491	1200	1819	1400
260	261	0.47	5.86	36	200	36	200
261	267	1.10	0.22	108	500	108	500
267	271	1.39	0.22	141	500	141	500

Table 4.1 Computed Street Sewer and Collector Discharges and Diameters (concluded)

From Node	To Node	Drained		Kinematic-wave		Hydrograph time-lag	
		Area ha	Slope %	Discharge lt/s	Diameter mm	Discharge lt/s	Diameter mm
276	277	0.18	8.22	3	200	3	200
277	271	0.49	5.66	38	200	38	200
271	250	2.73	0.23	220	600	220	600
289	250	0.26	2.85	31	200	31	200
108	109 <sub>z</sub>	0.32	1.28	40	250	40	250
109	250	0.85	3.37	104	300	104	300
114	115	0.37	1.60	46	250	46	250
115	117	1.22	2.48	153	350	153	350
250	302	19.57	0.71	2178	1200	2507	1400
117	302	2.31	2.13	289	500	289	500
40	303	0.16	5.19	12	200	12	200
303	308	0.58	5.87	25	200	25	200
308	313	0.91	5.96	63	200	63	200
313	317	1.13	4.50	88	250	88	250
317	320	1.30	2.54	97	300	97	300
329	330	0.31	0.74	12	200	12	200
330	320	0.57	0.75	42	300	42	300
320	332	2.55	0.53	220	500	220	500
332	337	3.20	0.18	296	700	296	700
337	342	3.64	0.19	346	800	346	800
302	350	22.21	2.42	2663	1200	2990	1400
342	350	3.93	2.26	382	800	382	800
354	355	0.07	3.94	8	200	8	200
355	360	0.48	4.02	14	200	14	200
360	370	1.15	1.75	63	250	63	250
370	371	1.25	0.78	64	300	64	300
371	372	1.67	2.50	117	300	117	300
372	350	2.23	2.62	187	350	187	350
350	400	29.30	2.20	3747	1200	4121	1400

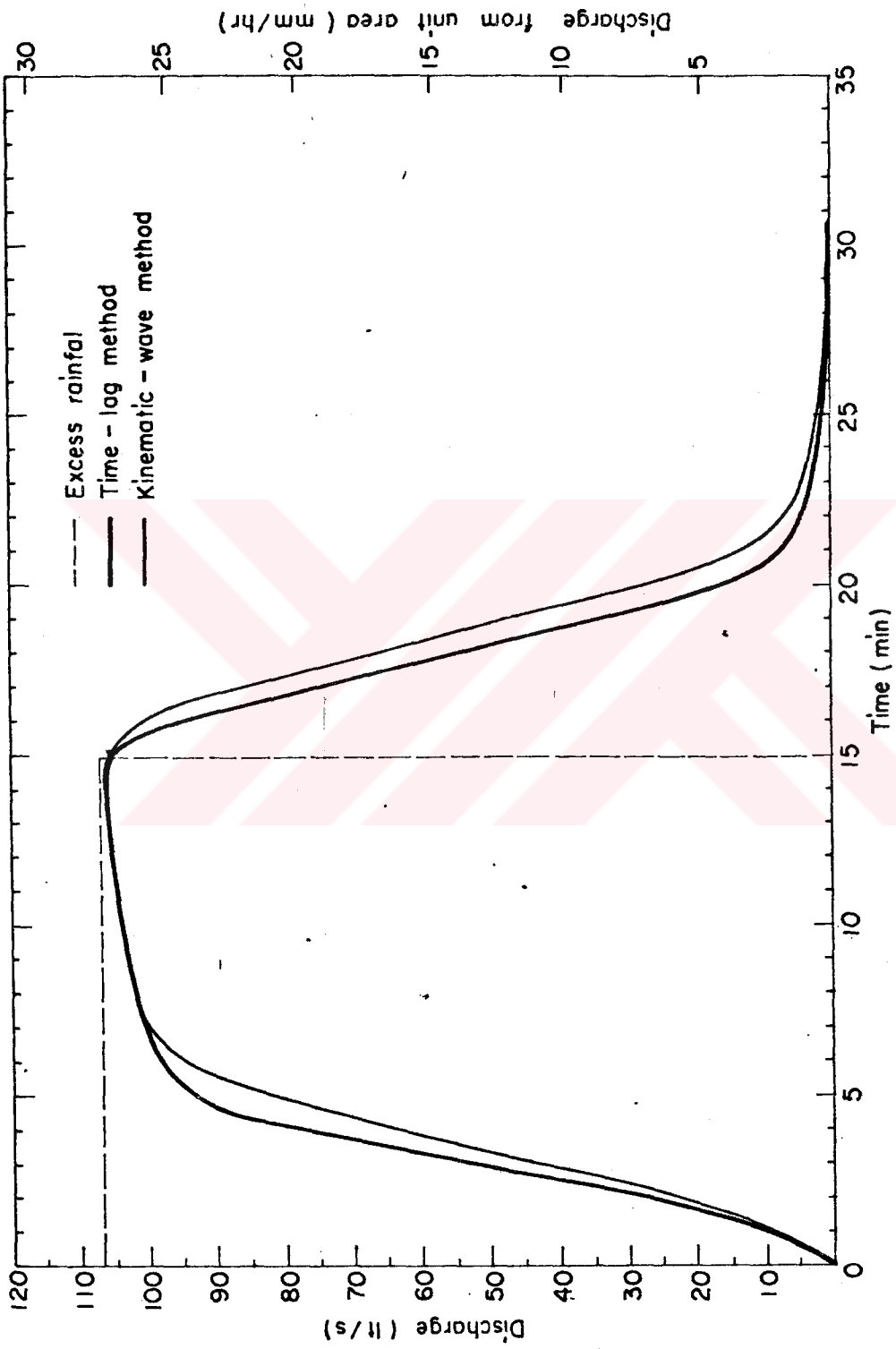


Fig. 4.2. Flow Hydrographs at Section 15



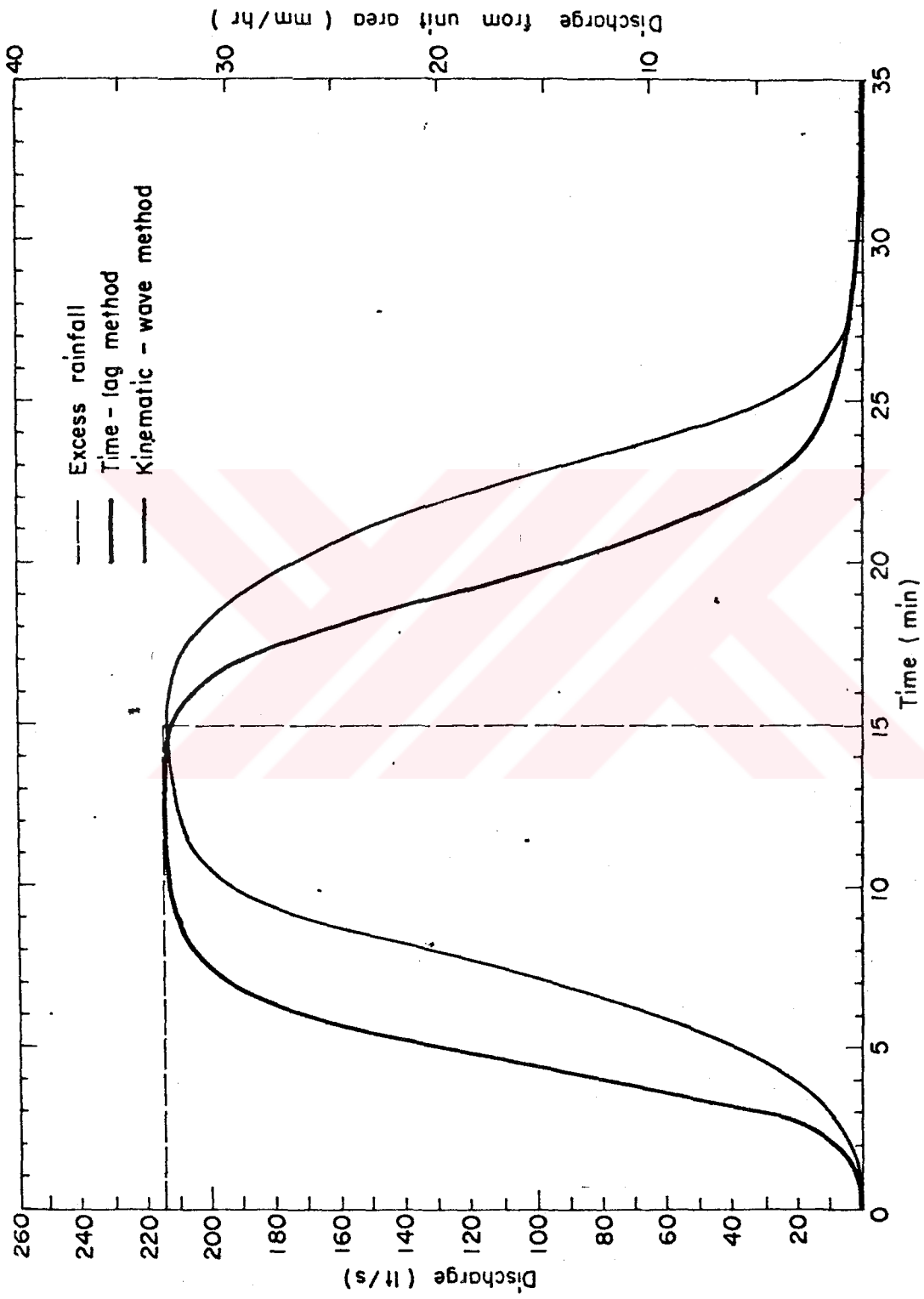


Fig. 4.3. Flow Hydrographs at Section 76

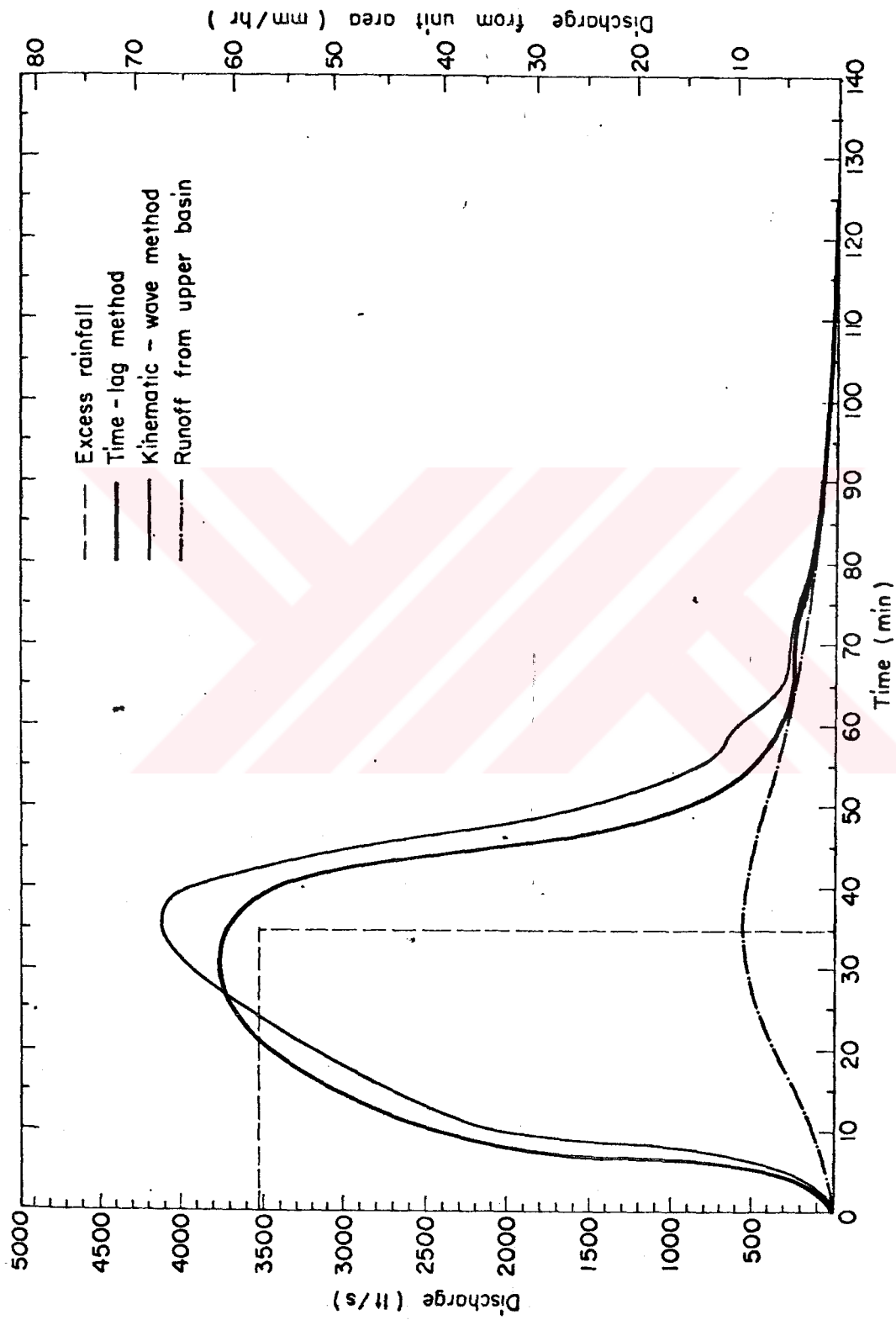


Fig. 4.4. Flow Hydrographs at Section 350

in the hydrograph time-lag method as shown in Fig. 4.4 of the hydrograph at section 350 along the collectors, and hence the sewer diameters are overestimated.

A comparison of the volumes under these hydrographs to that of excess rainfall indicates that continuity is satisfied within acceptable limits in the model. Errors concerning the flow continuity are listed in Table 4.2. The two schemes have comparable accuracy.

Table 4.2. Flow Continuity Errors

Flow Section	Excess Rainfall Volume $10^3 \text{ m}^3$	Hydrograph Time-Lag Method		Kinematic-Wave Method	
		Volume $10^3 \text{ m}^3$	Error %	Volume $10^3 \text{ m}^3$	Error %
15	96.1	96.5	1.7	94.9	1.2
76	193.3	198.0	2.4	196.9	1.9
350	7377.0	7788.9	5.7	7089.6	3.9

The execution time for the example application given here is 30 seconds for the hydrograph time-lag method and is 144 seconds for the simplified kinematic-wave scheme. The difference in the execution times of the two methods is mainly due to the use of smaller time steps in the kinematic-wave scheme required to overcome numerical stability problems.

## 5. CONCLUSIONS AND RECOMMENDATIONS

The most evident outcome of this study is a mathematical model and the corresponding computer program for the design of urban storm drainage systems. The mathematical model is not the most sophisticated one possible. It is rather a simple model which can be adopted in the real world problems without violating the basic principles of hydraulics.

The two options provided in the model concerning the flow routing in the sewer and collectors are hydrograph time-lag, and simplified kinematic-wave methods. The applications of these two schemes to drainage basin in the Batıkent area near Ankara, indicates that, as expectedly similar results can be obtained for sewers especially on the upstream portions of the basin. However, the sizes of the main collectors or the downstream sewers of large basins would be over estimated by the hydrograph time-lag method.

Additional options concerning the types of the sewers and the collectors as well as the system layout provides a reasonable flexibility for the model. Hence a variety of different types of storm drainage system can be designed by using the model developed.

The input data required by the model consists of variables most of which can easily be obtained from the maps of the drainage area under consideration. Engineering judgement may be necessary only in the selection of the abstraction indices and the design-storms. If no information is available on the abstraction indices a reasonable approach would be to set the index equal to zero for impervious surfaces directly connected to the drainage system, and set it equal to the storm intensity for pervious areas like gardens and lawns. A weighted abstraction index then can be computed for each subcatchment. As to the

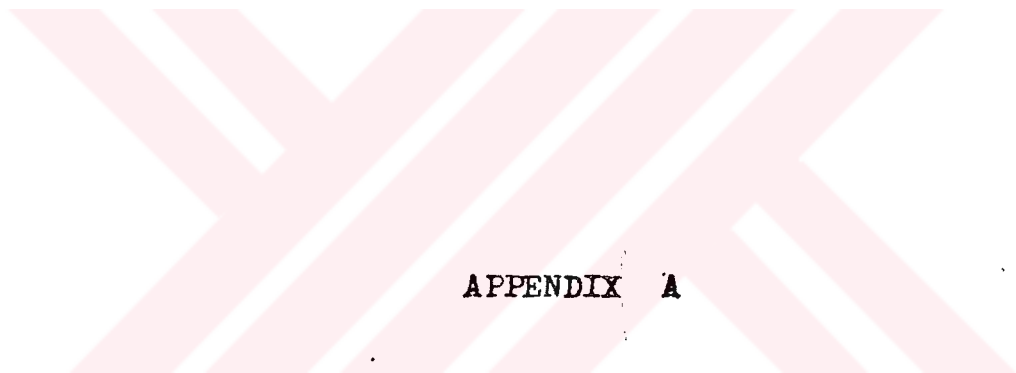
selection of the design-storms, it is suggested to try several combinations of the design-storms and select the couple which results in the most conservative design. Certainly the intensity and duration of these storms must be related through the intensity-duration-frequency curves for the region considered.



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APPENDIX A

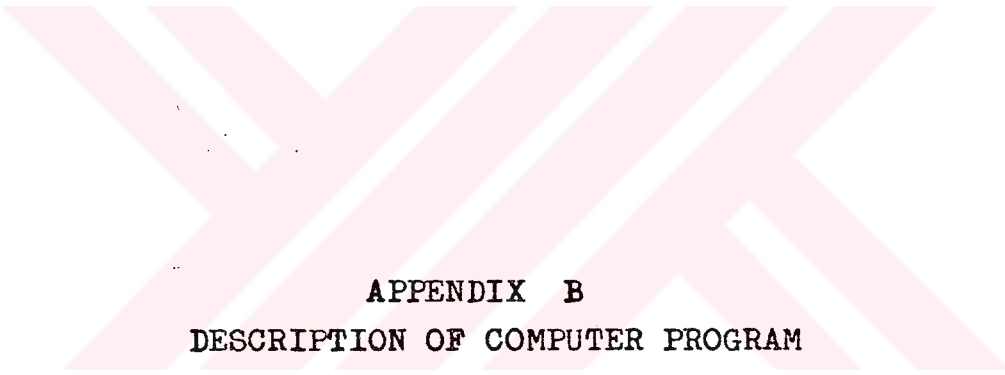


Table A.1. Values of  $n$  for Kinematic Wave Time of Concentration Formula (Yen, 1978)

Surface	$n$
Asphalt pavement	0.012
Concrete pavement	0.014
Bare packed soil	0.020
Rough bare packed soil	0.03
Mowed poor grass	0.03
Cultivated rows, no crop	0.03
Cultivated rows, with crop	0.04
Pasture-average grass	0.04
Dense grass	0.06
Shrubs and Brushes	0.08
Woods and forests	0.20
Land use	$n$
Business	0.015 - 0.030
Semi-business	0.020 - 0.035
Dense residential	0.025 - 0.040
Suburban residential	0.030 - 0.055
Parks	0.04 - 0.08
Light industrial	0.015 - 0.035

Table A.2. Values of Roughness Coefficient  $n$  of Manning  
Formula (ASCE and WPCF, 1969)

Conduit Material	Manning $n$
<b>Closed Conduits</b>	
Asbestos-cement pipe	0.011-0.015
Brick	0.013-0.017
Concrete (monolithic)	
Smooth forms	0.012-0.014
Rough forms	0.015-0.017
Concrete pipe	0.011-0.015
<b>Open Channels</b>	
<b>Lined channels</b>	
a. Asphalt	0.013-0.017
b. Brick	0.012-0.018
c. Concrete	0.011-0.020
d. Rubble or Riprap	0.020-0.035
e. Vegetal	0.030-0.040
<b>Excavated or Dregged</b>	
Earth, straight and uniform	0.020-0.030
Earth, winding fairly uniform	0.025-0.040
Rock	0.030-0.045
Unmaintained	0.050-0.14



**APPENDIX B**  
**DESCRIPTION OF COMPUTER PROGRAM**

## B. DESCRIPTION OF COMPUTER PROGRAM

In this chapter the computer program developed basing on the proposed mathematical model is described. In Section B.1, general features of the program are summarized. The major flow chart of the computer program is given in Section B.2. Then, Section B.3 is devoted to functioning of the main program and subroutines. The variables concerning the input data are described in Section B.4, whereas a description for preparing the input data is given in Section B.5. The deck and a sample output for the computer application of the model described in Chapter 4 are given as well as a listing of the computer program in Sections B.6, B.7, and B.8 respectively.

### B.1. General Features of Computer Program

The computer program developed for the mathematical model is coded in FORTRAN IV language. It consists of 1002 FORTRAN statements with a main program and seven subroutines. The storage requirement of the program is 126 K bytes approximately, and is independent of the number of the sewers to be considered at once. The computer program is general and can be applied to a variety of urban storm water drainage systems.

First subscript of matrices occurring in the common blocks and dimension statements of the program may need to be increased if the user prepares the data cards in an order deviating considerably from natural drainage pattern. Second subscript of the matrices and those of the vectors including characters "HYD" need to be increased if more than 250 time steps of computations are required.

The computer program terminates when input errors are detected, and computed section sizes are beyond the standard sizes specified for sewers and collectors.

The compilation time of the program for H-level/  
FORTRAN compiler on the IBM-SYSTEM 370/145 is 110 seconds.

## B.2. Major Flow Chart of Computer Program

The flow chart of the computer program developed for the mathematical model is given in Fig. B.1.

## B.3. Functions of Main Routine and Subprograms

Computer program is composed of a main program with seven subprograms and thirteen common blocks.

MAIN Program: All input data are read by the MAIN routine. The inputs are checked and a set of preliminary computations are performed and printed according to the option selections of the user. It also prints the design results in form of a table. The normal termination of the program is provided in the Main routine only.

Subprogram DESIGN: Determines the sections of sewers and collectors according to the peak discharges of inflow hydrographs by satisfying maximum allowable velocity criterion, and the heights of the chute structures if necessary. Subprogram also routes the hydrographs of sewers in the first-stage of design, and those of the collectors in the second-stage of design. Either hydrograph time-lag or simplified kinematic-wave method employed depending upon the selection of the user.

Subprogram HYDCAL: Determines the inlet hydrographs in the first-stage of design, and also computes the overland flow hydrographs in the second-stage of design. These hydrographs are of trapezoidal and triangular shapes as discrete ordinates at equal time intervals which specified by the user.

Subprogram TOPLAM: Determines the discharge intercepted by a gutter inlet and the carry-over in the second-stage of design.

Subprogram RATIO: Determines the required number of the additional inlets between those initially placed to

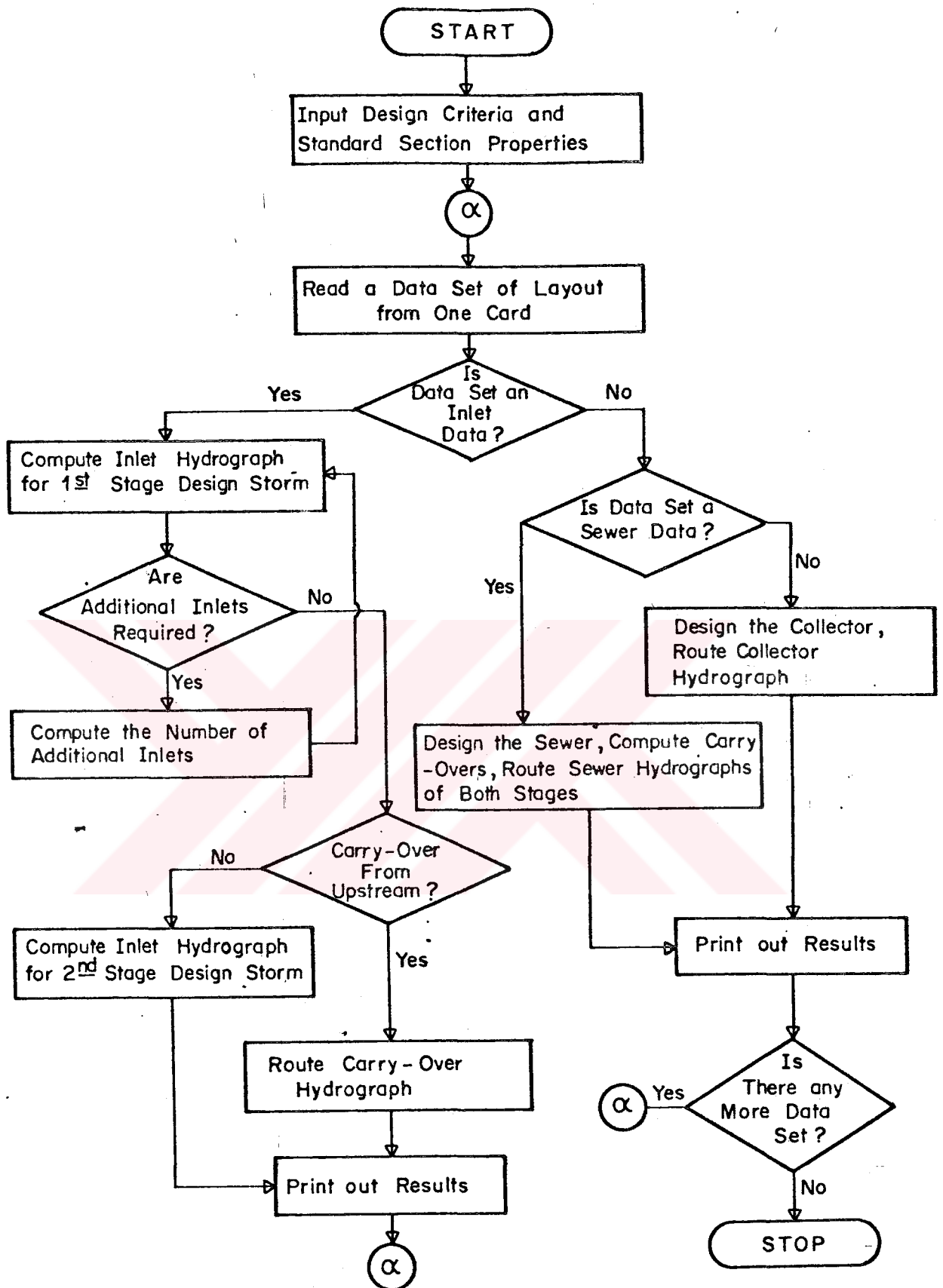


Fig. B.1. Major Flow Chart of Computer Program

keep the gutter discharge and flow depth below the specified limits.

Subprogram SIMULM: Routes the sewer hydrograph in the second-stage of design by one of the schemes, hydrograph time-lag or simplified kinematic-wave methods.

Subprogram ROUTE: Performes gutter flow routing by summing carry-over and surface runoff hydrographs in the second-stage of design.

Subprogram YNORM: Calculates the normal flow depth corresponding to a specified discharge and channel geometry in rectangular and trapezoidal canals by an iteration technique.

#### B.4. Description of Input Variables

The user should provide the data for the input variables described below:

- TITLE : Title of the design problem which appears on the top of the program output.
- JK : The number of hydrographs that need to be stored, and should be small than the first subscript of matrices.
- IJK : Total number of time steps which should be small than the second subscript of matrices and dimension of vectors containing characters "HYD".
- IDES : Number of segments which a gutter is divided for carry-over routing, and should be large than zero.
- IROUTE : Selection for routing scheme to be adopted for flow in sewers and collectors.  
≠0 : Simplified kinematic-wave method is selected.  
=0 : Hydrograph time-lag method is selected.
- ISTEP : Number of subdivisions of the time increment DELT which to be employed in simplified kinematic-wave routing.

ITR : Return period for the design of first-group elements (Years).  
 JTR : Return period for the design of second-group elements (Years).  
 NCANAL : Number of standard rectangular sections.  
 NPIPE : Number of standard circular sections.  
 NTRAP : Number of standard trapezoidal sections.  
 NMEC : Number of sewers under a street. 1 or 2.  
 NSECA : Selection of section type for the design of sewers.  
       =0 : Circular sections,  
       =1 : Rectangular sections.  
 NSECB : Selection of section type for the design of collectors.  
       =0 : Circular sections,  
       =1 : Rectangular sections,  
       =2 : Trapezoidal sections.  
 NART : Maximum number of larger section sizes tried as an alternative chute structures.  
 LMIN : Standard section type number below which a list of the computed sewer sizes can optionally be obtained.  
 AINTA : Rainfall intensity for the design of first-group elements (mm/hr).  
 AINTB : Rainfall intensity for the design of second-group elements (mm/hr).  
 TDA : Rainfall duration for AINTA (min).  
 TDB : Rainfall duration for AINTB (min).  
 VMAX : Maximum allowable velocity for sewers (m/s).  
 QMAX : Maximum allowable gutter discharge (lt/s).  
 YMAX : Maximum allowable gutter flow depth (cm).



VMAXB : Maximum allowable velocity for collectors (m/s).  
 DELT : Time increment for hydrographs (min).  
 GUTRZ : Reciprocal of street crown slope.  
 GUTRN : Manning roughness factor for gutters.  
 CANALN : Manning roughness factor for rectangular sections.  
 PIPEN : Manning roughness factor for circular sections.  
 TRAPN : Manning roughness factor for trapezoidal sections.  
 DROP : Minimum soil cover for pipes (m)  
 RATK : Maximum depth ratio for rectangular sections.  
 RATT : Maximum depth ratio for trapezoidal sections.  
 TYPEA  
 (I,J) : Dimensions of standard rectangular sections.  
           J=1,NCANAL  
           I=1 : Width of the section (m),  
           I=3 : Height of the section (m).  
 TYPEB(I) : Diameters of standard circular sections (mm)  
           I=1,NPIPE  
 TYPEC  
 (I,J) : Dimensions of standard trapezoidal sections  
           J=1,NTRAP  
           I=1 : Bottom width of the section (m),  
           I=2 : Side slope of the section (m/m),  
           I=3 : Height of the section (m).  
 ITH : Upstream node number.  
 KP : Upstream node condition.  
       =Ø : Upstream end of a gutter of most extreme  
           inlet,  
       =I : Inlet,  
       =M : Manhole on a sewer,  
       =B : Inflow to a collector junction from upper  
           basin,  
       =P : Collector junction.

JTH : Downstream node number.  
 KR : Downstream node condition.  
     =I : Inlet,  
     =M : Manhole on a sewer,  
     =P : Collector junction.  
 AREA : Area of the subcatchment or exterior drainage area (ha).  
 ALEN : Length of the gutter, street sewer or collector between the nodes ITH and JTH (m).  
 AELEV : Upstream node topographic elevation (m).  
 BELEV : Downstream node topographic elevation (m).  
 PHY : Abstraction index for the subcatchment (mm/hr)  
 AN : Manning roughness factor of the subcatchment.  
 SLOPY : Average slope of the subcatchment (m/m).  
 ALENY : Length of the drain path of the subcatchment (m).  
 LP : Index indicating if the computed inflow hydrograph at a node is desired to be printed out,  
     ≠0 : Hydrograph is desired,  
     =0 : Hydrograph is not desired.  
 NODI,  
     NODJ : Node numbers of inlets from which carry-over is delivered directly into a downstream gutter. Also, NODJ represent the total number of ordinates of upper basin hydrograph if KP is defined as B.  
 HYD(I,J): Upper basin hydrograph ordinates (lt/s).  
     I=1,NODJ

### B.5. Preparation of Data

Information on the design criteria, standard section sizes, basin characteristics and the drainage pattern of the urban area must be prepared by the user. Also he should number all the inlets, manholes, sewer and

collector junctions; and optionally the upstream ends of all the exterior gutters. Numbering can be done arbitrarily but each number should be used only once. Each data card contains all the information necessary about the drainage area, or the sewer between the numbered points depending upon whether these numbers represent inlets or sewers. The user should also specify the inlet-manhole connections.

The data deck for the computer program can be classified into four groups containing information on:

- a. Design criteria,
- b. Standard sewer and collector section sizes,
- c. Description of the layout following the drainage pattern
- d. Upper basin hydrograph(s).

Data Set a

This data set is supplied in subsets to be given in the order of a1, a2, a3, a4.

Subset a1 : This subset contains of 3 cards on which the variable TITLE is written in alphanumeric characters on 1-80 columns of each card.

Subset a2 : This subset consists of a single card and contains the following inputs.

<u>Variable Name</u>	<u>Type of Variable</u>	<u>Columns</u>
JK	Integer	1- 5
IJK	Integer	6-10
IDES	Integer	11-15
IROUTE	Integer	16-20
ISTEP	Integer	21-25

If IROUTE is zero, ISTEP does not have to be defined.

Subset a3 : This subset contains of a single card and contains the following inputs.

<u>Variable Name</u>	<u>Type of Variable</u>	<u>Columns</u>
ITR	Integer	1- 5
JTR	Integer	6-10
NCANAL	Integer	11-15
NPIPE	Integer	16-20
NTRAP	Integer	21-25
NMEC	Integer	26-30
NSECA	Integer	31-35
NSECB	Integer	36-40
NART	Integer	41-45
LMIN	Integer	46-50

The variable NPIPE is defined if NSECA=0 and/or NSECB=0. The variable NCANAL is defined if NSECA=1 and/or NSECB=1. The variable NTRAP must be defined if NSECB=2.

Subset a4 : This subset consists of three cards and contains the following inputs.

First card of subset a4:

<u>Variable Name</u>	<u>Type of Variable</u>	<u>Columns</u>
AINTA	Real	1-10
AINTB	Real	11-20
TDA	Real	21-30
TDB	Real	31-40
VMAX	Real	41-50
QMAX	Real	51-60
YMAX	Real	61-70
VMAXB	Real	71-80

Second card of subset a4:

<u>Variable Name</u>	<u>Type of Variable</u>	<u>Columns</u>
DELT	Real	1-10
GUTRZ	Real	11-20
GUTRN	Real	21-30
CANALN	Real	31-40
PIPEN	Real	41-50
TRAPN	Real	51-60
DROP	Real	61-70
RATK	Real	71-80

Third card of subset a4:

<u>Variable Name</u>	<u>Type of Variable</u>	<u>Columns</u>
RATT	Real	1-10

The variable PIPEN is defined if NSECA = 0 and/or NSECB = 0. The variable CANALN is defined if NSECA = 1 and/or NSECB = 1. The variable TRAPN must be defined if NSECB = 2. Also, the variable RATK is defined if NSECA = 1 or NSECB = 1. The variable RATT must be defined if NSECB = 2.

#### Data Set b

This data set is to be given in three subsets in the order of b1, b2, b3.

Subset b1 : This subset must be provided if NCANAL already given is greater than zero. Otherwise this subset must be omitted. The number of cards in this subset can be computed by truncating the result of  $(NCANAL/8 + 1)$ . This subset contains the following inputs.

<u>Variable Name</u>	<u>Type of Variable</u>	<u>Columns</u>
TYPEA(1,1)	Real	1-5
TYPEA(3,1)	Real	6-10

<u>Variable Name</u>	<u>Type of Variable</u>	<u>Columns</u>
TYPEA(1,2)	Real	11-15
TYPEA(3,2)	Real	16-20
.....	Real	.....
.....	Real	.....
TYPEA(1,NCANAL)	Real	.....
TYPEA(3,NCANAL)	Real	.....

Subset b2 : This subset must be provided if NPIPE already given is greater than zero. Otherwise it must be omitted. The number of cards in this subset can be computed by truncating the result of  $(NPIPE/16 + 1)$ .

This subset contains the following inputs.

<u>Variable Name</u>	<u>Type of Variable</u>	<u>Columns</u>
TYPEB(1)	Real	1-5
TYPEB(2)	Real	6-10
TYPEB(3)	Real	11-15
.....	Real	.....
.....	Real	.....
TYPEB(NPIPE-1)	Real	.....
TYPEB(NPIPE)	Real	.....

Subset b3 : This subset must be provided if NTRAP already given is greater than zero. Otherwise it must be omitted. The number of cards in this subset can be computed by truncating the result of  $(NTRAP \times 3 / 16 + 1)$ .

This subset contains the following inputs.

<u>Variable Name</u>	<u>Type of Variable</u>	<u>Columns</u>
TYPEC(1,1)	Real	1-5
TYPEC(2,1)	Real	6-10
TYPEC(3,1)	Real	11-15

<u>Variable Name</u>	<u>Type of Variable</u>	<u>Columns</u>
TYPEEC(1,2)	Real	16-20
TYPEEC(2,2)	Real	21-25
TYPEEC(3,2)	Real	26-30
.....	Real	.....
.....	Real	.....
.....	Real	.....
TYPEEC(1,NTRAP)	Real	.....
TYPEEC(2,NTRAP)	Real	.....
TYPEEC(3,NTRAP)	Real	.....

#### Data Set c

This data set contains information about catchments, and sewer layout. For each inlet, there are two cards. The first one contains the contributing subcatchment characteristics, and the second one indicates what manhole the inlet is connected to. Also there will be a single card for each sewer and each collector. Additional cards may be needed each corresponding to a junction on the collector which receives direct inflow from upper basins.

Each card of data set c contains the following inputs.

<u>Variable Name</u>	<u>Type of Variable</u>	<u>Columns</u>
ITH	Integer	1-44
KP	Alphanumeric	5
JTH	Integer	6-9
KR	Alphanumeric	10
AREA	Real	11-16
ALEN	Real	17-22
AELEV	Real	23-28

<u>Variable Name</u>	<u>Type of Variable</u>	<u>Columns</u>
BELEV	Real	29-36
PHY	Real	37-42
AN	Real	43-48
SLOPY	Real	49-54
ALENY	Real	55-60
LP	Integer	69-72
NODI	Integer	73-76
NODJ	Integer	77-80

On each card of this data set ITH, KP, JTH, and KR must always be defined. If KP and KR are defined both as M; or respectively as M and P; the variables other than AELEV, BELEV, NODI, and NODJ need not to be defined. If KP and KR are defined both as P, the variables other than AELEV and BELEV need not to be defined. The variable LP is defined in cases that the design flow hydrograph is desired at section ITH. If KP and KR are defined respectively as I and M; variables other than ITH and JTH need not to be defined. If KP and KR are defined respectively as B and P; AREA and NODJ should be defined in addition to ITH and JTH.

If a card contains KP defined as B then a set of cards described in data set d are placed between this particular card and the following one.

#### Data Set d

This data set must be provided inside the data set c each time a card in data set c has KP defined as B. The set d is placed after the related card. The number of cards in this data set can be computed by truncating the result of  $(NODJ/8+1)$ ; and contains the following inputs.



<u>Variable Name</u>	<u>Type of Variable</u>	<u>Columns</u>
HYD(I,1)	Real	1-10
HYD(I,2)	Real	11-20
HYD(I,3)	Real	21-30
.....	Real	.....
.....	Real	.....
HYD(I,NODJ)	Real	.....

I is a variable defined by the model and not related to input data.



**B.6. INPUT DATA DECK**

1	2	3	4	5	6	7	8
APPLICATION OF THE MODEL TO							
BAYKENT SATELLITE TOWN AREA							
NEAR ANKARA							
10	16	1C	0	2			
68.	15.	15.	07.	0.016		7.	15.
1.30	30.	0.02				1.	0.75
1.75	1.75	1.00	2.15	2.20	2.55	3.50	4.50
1.50	1.75	1.75	2.00	2.20	2.50	3.00	3.05
20.00	4.50	4.50	700.	1000.	1200.	1400.	1600.
0.50	3.50	3.50	0.75	0.90	1.00	1.00	1.00
1.50	1.50	1.50	1.25	1.50	1.50	1.50	1.25
1.70	1.00	1.00	0.04	0.05	0.04	0.04	0.04
79	3110.00	3110.00	0.04	0.05	0.04	0.04	0.04
80	32M	32M					
81M	33M	33M					80
82M	34M	34M					
83M	35M	35M					
84M	36M	36M					
85M	37M	37M					
86M	38M	38M					
87M	39M	39M					
88M	40M	40M					
89M	41M	41M					
90M	42M	42M					
91M	43M	43M					
92M	44M	44M					
93M	45M	45M					
94M	46M	46M					
95M	47M	47M					
96M	48M	48M					
97M	49M	49M					
98M	50M	50M					56
99M	51M	51M					50
1	2	3	4	5	6	7	8
1	2	3	4	5	6	7	8
1	2	3	4	5	6	7	8

1	2	3	4	5	6	7	8
5M	45:	865:54868:72	0:040	0:1C			DATA
11M	45:	865:54868:72	0:040	C:5C			DATA
12M	78:	875:54868:72	C:040	C:02			DATA
13M	78:	875:54868:72					DATA
14M							DATA
15M	47:	868:72867:12	0:040	0:07			DATA
16M	47:	868:72867:12	0:040	C:02			DATA
17M	78:	877:11867:12	0:040	C:02			DATA
18M	78:	877:11867:12					DATA
19M	46:	867:12865:42	0:040	C:02			DATA
20M	78:	871:48865:42	0:040	C:02			DATA
21M	78:	871:48865:42	0:040	C:02			DATA
22M	46:	867:12865:42					DATA
23M							DATA
24M	46:	865:42862:85	0:040	0:06			DATA
25M	46:	865:42862:85	0:040	C:1C			DATA
26M	77:	865:70862:85	0:040	C:02			DATA
27M	77:	865:70862:85					DATA
28M							DATA
29M	46:	862:85861:74	0:040	C:02			DATA
30M	46:	862:85861:74					DATA
31M							DATA
32M	44:	861:74861:46	0:040	C:05			DATA
33M	77:	861:74861:46	0:040	C:02			DATA
34M	77:	861:74861:46	0:040	C:02			DATA
35M	45:	875:54868:72					DATA
36M							DATA
37M	45:	877:11867:12	0:040	C:25			DATA
38M	45:	877:11867:12					DATA
39M							DATA
40M							DATA
41M							DATA
42M							DATA
43M							DATA
44M							DATA
45M							DATA
46M							DATA
47M							DATA
48M							DATA
49M							DATA
50M							DATA
51M							DATA
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66M							DATA
67M							DATA
68M							DATA
69M							DATA
70M							DATA
71M							DATA
72M							DATA
73M							DATA
74M							DATA
75M							DATA
76M							DATA
77M							DATA
78M							DATA
79M							DATA
80M							DATA

.....1.....2.....3.....4.....5.....6.....7.....8

44I	43M	87E	11E71.48	27.	0.04	C.20	57.	DATA	81
45I	46M	87E	11E71.48	27.	0.04	C.20	57.	DATA	82
46I	47M	87E	11E71.48	27.	0.04	C.20	57.	DATA	83
47I	48M	87E	11E71.48	27.	0.04	C.20	57.	DATA	84
48I	49M	87E	11E71.48	27.	0.04	C.20	57.	DATA	85
49I	50M	87E	11E71.48	27.	0.04	C.20	57.	DATA	86
50I	51M	87E	11E71.48	27.	0.04	C.20	57.	DATA	87
51I	52M	87E	11E71.48	27.	0.04	C.20	57.	DATA	88
52I	53M	87E	11E71.48	27.	0.04	C.20	57.	DATA	89
53I	54M	87E	11E71.48	27.	0.04	C.20	57.	DATA	90
54I	55M	87E	11E71.48	27.	0.04	C.20	57.	DATA	91
55I	56M	87E	11E71.48	27.	0.04	C.20	57.	DATA	92
56I	57M	87E	11E71.48	27.	0.04	C.20	57.	DATA	93
57I	58M	87E	11E71.48	27.	0.04	C.20	57.	DATA	94
58I	59M	87E	11E71.48	27.	0.04	C.20	57.	DATA	95
59I	60M	87E	11E71.48	27.	0.04	C.20	57.	DATA	96
60I	61M	87E	11E71.48	27.	0.04	C.20	57.	DATA	97
61I	62M	87E	11E71.48	27.	0.04	C.20	57.	DATA	98
62I	63M	87E	11E71.48	27.	0.04	C.20	57.	DATA	99
63I	64M	87E	11E71.48	27.	0.04	C.20	57.	DATA	100
64I	65M	87E	11E71.48	27.	0.04	C.20	57.	DATA	101
65I	66M	87E	11E71.48	27.	0.04	C.20	57.	DATA	102
66I	67M	87E	11E71.48	27.	0.04	C.20	57.	DATA	103
67I	68M	87E	11E71.48	27.	0.04	C.20	57.	DATA	104
68I	69M	87E	11E71.48	27.	0.04	C.20	57.	DATA	105
69I	70M	87E	11E71.48	27.	0.04	C.20	57.	DATA	106
70I	71M	87E	11E71.48	27.	0.04	C.20	57.	DATA	107
71I	72M	87E	11E71.48	27.	0.04	C.20	57.	DATA	108
72I	73M	87E	11E71.48	27.	0.04	C.20	57.	DATA	109
73I	74M	87E	11E71.48	27.	0.04	C.20	57.	DATA	110
74I	75M	87E	11E71.48	27.	0.04	C.20	57.	DATA	111
75I	76M	87E	11E71.48	27.	0.04	C.20	57.	DATA	112
76I	77M	87E	11E71.48	27.	0.04	C.20	57.	DATA	113
77I	78M	87E	11E71.48	27.	0.04	C.20	57.	DATA	114
78I	79M	87E	11E71.48	27.	0.04	C.20	57.	DATA	115
79I	80M	87E	11E71.48	27.	0.04	C.20	57.	DATA	116
80I	81M	87E	11E71.48	27.	0.04	C.20	57.	DATA	117
81I	82M	87E	11E71.48	27.	0.04	C.20	57.	DATA	118
82I	83M	87E	11E71.48	27.	0.04	C.20	57.	DATA	119
83I	84M	87E	11E71.48	27.	0.04	C.20	57.	DATA	120

35

60

57

1	2	3	4	5	6	7	8
777B	777P	5	20	70	50	55	DATA
215	100	120	130	205	225	24	DATA
245	100	150	135	205	240	45	DATA
453	100	550	515	430	460	53	DATA
445	100	550	548	490	465	45	DATA
340	100	513	400	483	368	55	DATA
348	100	413	305	353	328	55	DATA
100	100	218	210	250	195	26	DATA
173	100	158	215	200	148	33	DATA
173	100	115	105	148	143	13	DATA
439	100	435	160	155	186	55	DATA
426	100	435	40	388	335	30	DATA
16	100	214	24	21	21	25	DATA
779	78P	862.84	0.04	C.C1	1	75	DATA
75M	76M	860.21	0.04	C.C2	1	75	DATA
76M	78P	860.21	0.04	C.C2	1	75	DATA
78M	78P	860.21	0.04	C.C2	1	75	DATA
62M	70P	857.74	0.04	C.C5	66	69	DATA
66M	70P	857.74	0.04	C.C2	66	69	DATA
69P	70P	857.74	0.04	C.C2	66	69	DATA
70P	70P	857.74	0.04	C.C2	66	69	DATA
102M	102M	864.47	0.04	C.C1	1	102	DATA
103M	103M	864.43	0.04	C.C1	1	102	DATA
104M	104M	864.43	0.04	C.C2	21	107	DATA
107M	107M	864.43	0.04	C.C2	21	107	DATA
104M	100P	858.53	0.04	C.C3	41	201	DATA
107M	101M	858.53	0.04	C.C3	41	201	DATA
100M	201M	872.11	0.04	C.C5	16	201	DATA
202M	202M	872.11	0.04	C.C5	16	201	DATA
201M	204M	872.11	0.04	C.C1	47	201	DATA
2015	206M	872.11	0.04	C.C1	47	201	DATA
207	208M	877.11	0.04	C.C4	47	201	DATA
207	209M	877.11	0.04	C.C4	47	201	DATA

1	2	3	4	5	6	7	8
203M							161
203M							162
203M	47.	868.84885.57					163
204M	46.	868.57883.06					164
204M	90.	868.57883.06	0.04	C.04			165
209M			0.02	C.04			166
211M	46.	868.57883.06					167
211M	46.	868.57883.06					168
211M			0.04	0.02			169
211M							170
211M							171
211M							172
211M							173
211M							174
211M							175
211M	71.	868.57883.06					176
211M	71.	868.57883.06	0.04	C.04			177
211M	71.	868.57883.06	0.04	C.02			178
211M	140.	868.57883.06					179
211M	90.	868.57883.06	0.02	C.01			180
211M	90.	868.57883.06	0.06	C.06			181
211M	45.	868.57883.06	0.06	C.07			182
211M	45.	868.57883.06	0.04	C.03			183
211M	47.	868.57883.06	0.02	C.03			184
211M	47.	868.57883.06	0.04	C.02			185
211M							186
211M							187
211M							188
211M							189
211M							190
211M							191
211M							192
211M							193
211M							194
211M							195
211M							196
211M							197
211M							198
211M							199
211M							200
266M	46.	868.57883.06					209
266M	46.	868.57883.06					204
266M							213
266M							212
266M							215
266M							256
266M							259
266M							191
266M							192
266M							193
266M							194
266M							195
266M							196
266M							197
266M							198
266M							199
266M							200

1	2	3	4	5	6	7	8
254	80:	864.233856.20	27:	0.04	C.C4	15.	DATA 202
255	80:	864.233856.20	27:	0.04	C.C4	15.	DATA 203
260	45:	856.2 856.1	27:	0.04	C.C4	18.	DATA 204
261	45:	856.2 856.1	27:	0.04	C.C4	18.	DATA 205
262	91:	871.76864.33	63:	0.06	C.C75	40.	DATA 206
263	45:	864.233860.63	27:	0.04	C.C8	22.	DATA 207
264	45:	864.233860.63	27:	0.04	C.C7	17.	DATA 208
265	40:	861.25860.63	27:	0.04	C.C2	15.	DATA 209
266	41:	861.25860.63	27:	0.04	C.C2	15.	DATA 210
267	80:	860.63856.10	27:	0.04	C.C5	22.	DATA 211
268	80:	860.63856.10	27:	0.04	C.C5	22.	DATA 212
269	43:	856.10856.00	27:	0.04	C.C5	61.	DATA 213
270	43:	856.10856.00	27:	0.04	C.C5	61.	DATA 214
271	48:	858.25858.31	27:	0.04	C.C4	38.	DATA 215
272	43:	858.25858.31	27:	0.03	C.C2	23.	DATA 216
273	81:	858.21856.00	63:	0.06	C.C4	33.	DATA 217
274	81:	858.21856.00	63:	0.03	C.C3	19.	DATA 218
275	91:	864.43858.34	23:	0.03	C.C3	19.	DATA 219
276	108M	859.24858.09	23:	0.03	C.C5	20.	DATA 220
277	108M	859.24858.09	23:	0.03	C.C5	20.	DATA 221
278	110IC.28						DATA 222
279	110IC.28						DATA 223
280	110IC.28						DATA 224
281	110IC.28						DATA 225
282	110IC.28						DATA 226
283	110IC.28						DATA 227
284	110IC.28						DATA 228
285	110IC.28						DATA 229
286	110IC.28						DATA 230
287	110IC.28						DATA 231
288	110IC.28						DATA 232
289	110IC.28						DATA 233
290	110IC.28						DATA 234
291	110IC.28						DATA 235
292	110IC.28						DATA 236
293	110IC.28						DATA 237
294	110IC.28						DATA 238
295	110IC.28						DATA 239
296	110IC.28						DATA 240



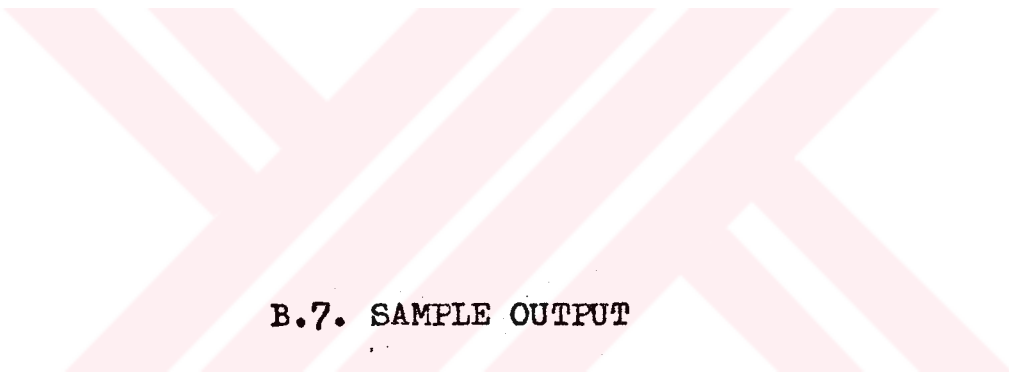
1	2	3	4	5	6	7	8
112V	0.25	59.	0.04	0.05	24.		DATA 241
112M		59.	0.04	0.05	24.		DATA 242
112P		62.					DATA 243
112M	0.31	62.	0.04	0.06	108.	110	DATA 244
112P	0.37	100.	0.03	0.02	32.		DATA 245
113M		128.					DATA 246
113P	0.85	128.	0.03	0.05	111.	113	DATA 247
113M		101.					DATA 248
113P	0.75	101.	0.03	0.05	111.	116	DATA 249
113M	0.69	61.	0.03	0.04	25.		DATA 250
113P	0.25	61.	0.03	0.03	22.		DATA 251
113M		95.					DATA 252
113P		108.					DATA 253
113M	0.33	43.	0.03	0.03	55.	301	DATA 254
113P	0.06	43.	0.04	0.07	24.		DATA 255
113M	0.01	45.	0.04	0.03	24.		DATA 256
113P		57.					DATA 257
113M	0.14	46.	0.06	0.06	39.	37	DATA 258
113P	0.20	82.	0.06	0.05	43.		DATA 259
113M	0.08	82.	0.04	0.02	12.		DATA 260
113P		45.					DATA 261
113M	0.07	45.	0.04	0.05	21.	307	DATA 262
113P	0.15	82.	0.04	0.04	26.		DATA 263
113M	0.11	82.	0.04	0.03	21.		DATA 264
113P		45.					DATA 265
113M	0.06	45.	0.04	0.04	22.	312	DATA 266
113P							DATA 267
113M							DATA 268
113P							DATA 269
113M							DATA 270
113P							DATA 271
113M							DATA 272
113P							DATA 273
113M							DATA 274
113P							DATA 275
113M							DATA 276
113P							DATA 277
113M							DATA 278
113P							DATA 279
113M							DATA 280

1	2	3	4	5	6	7	8
316	10.16	126.	871.24	862.84	27.	9.04	C.02 10.
317							
318							
319							
320							
321							
322							
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400							

.....1.....2.....3.....4.....5.....6.....7.....8

333	336	DATA	11
333	336	DATA	12
333	336	DATA	13
333	336	DATA	14
333	336	DATA	15
333	336	DATA	16
333	336	DATA	17
333	336	DATA	18
333	336	DATA	19
333	336	DATA	20
333	336	DATA	21
333	336	DATA	22
333	336	DATA	23
333	336	DATA	24
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333	336	DATA	26
333	336	DATA	27
333	336	DATA	28
333	336	DATA	29
333	336	DATA	30
333	336	DATA	31
333	336	DATA	32
333	336	DATA	33
333	336	DATA	34
333	336	DATA	35
333	336	DATA	36
333	336	DATA	37
333	336	DATA	38
333	336	DATA	39
333	336	DATA	40
333	336	DATA	41
333	336	DATA	42
333	336	DATA	43
333	336	DATA	44
333	336	DATA	45
333	336	DATA	46
333	336	DATA	47
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333	336	DATA	67
333	336	DATA	68
333	336	DATA	69
333	336	DATA	70
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333	336	DATA	78
333	336	DATA	79
333	336	DATA	80
333	336	DATA	81
333	336	DATA	82
333	336	DATA	83
333	336	DATA	84
333	336	DATA	85
333	336	DATA	86
333	336	DATA	87
333	336	DATA	88
333	336	DATA	89
333	336	DATA	90
333	336	DATA	91
333	336	DATA	92
333	336	DATA	93
333	336	DATA	94
333	336	DATA	95
333	336	DATA	96
333	336	DATA	97
333	336	DATA	98
333	336	DATA	99
333	336	DATA	100

.....1.....	.....2.....	.....3.....	.....4.....	.....5.....	.....6.....	.....7.....	.....8
3681 372M	107: 85E.CC852.20		1				DATA 361
372M 350P	107: 85E.CC852.20	23.	0.03	C.C4	59.		368 DATA 362
3681 350P	10C: 852.20850.CC					1	DATA 363
350P 400P							DATA 364
.....1.....	.....2.....	.....3.....	.....4.....	.....5.....	.....6.....	.....7.....	.....8



**B.7. SAMPLE OUTPUT**

\*\*\*\*\*  
 APPLICATION OF THE MODEL TO  
 EASTKENT SATELLITE TOWN AREA  
 NEAR ANKARA  
 \*\*\*\*\*

\*\*\*\*\* DESIGN CRITERIA \*\*\*\*\*  
 RECURRENCE PERIOD FOR SEWERS..... =  
 RECURRENCE PERIOD FOR COLLECTORS..... =  
 RAINFALL DURATION FOR COLLECTORS..... =  
 RAINFALL INTENSITY FOR COLLECTORS..... =  
 RAINFALL INTENSITY FOR SEWERS..... =  
 ALLOWABLE MAX. VELOCITY IN COLLECTORS..... =  
 ALLOWABLE MAX. VELOCITY IN GUTTERS..... =  
 MAX. FLOW RATE IN GUTTERS..... =  
 MAX. FLOW DEPTH IN GUTTERS..... =  
 CROSS-SECTIONAL SLOPE OF GUTTERS..... =  
 MINIMUM ROUGHNESS COEF. IN GUTTERS..... =  
 TIME INCREMENT FOR HYDROGRAPHS..... =  
 MIN. SIZE FOR PIPES..... =  
 MAX. NUMBER OF LARGER SECTION SIZES TRIED..... =  
 AS AN ALTERNATIVE TO CHUTE STRUCTURES..... =  
 YEAR..... 5  
 YEAR..... 25  
 MIN..... 15.0  
 MM/HOUR..... 35.0  
 MM/HOUR..... 68.0  
 MM/SEC..... 87.0  
 M/SEC..... 15.0  
 L/SEC..... 50.0  
 CM..... 7.0  
 MIN..... 0.020  
 METER..... 0.020  
 MIN..... 1.00  
 METER..... 1.00  
 2

\*\*\*\*\*  
 HYDROGRAPH TIME LAG METHOD IS SELECTED  
 \*\*\*\*\*

\*\*\*\*\*ONLY CIRCULAR PIPES WILL BE USED FOR SEWERS\*\*\*\*\*

NUMBER OF STANDARD DIAMETERS : 16  
MANNING ROUGHNESS COEFFICIENT FOR PIPES : 0.016  
MAXIMUM RATIO OF DEPTH TO DIAMETER : 0.900

PIPE	:	1	:	200.	MM
TYPE	:	2	:	250.	MM
PIPE	:	3	:	300.	MM
TYPE	:	4	:	350.	MM
PIPE	:	5	:	400.	MM
TYPE	:	6	:	500.	MM
PIPE	:	7	:	600.	MM
TYPE	:	8	:	700.	MM
PIPE	:	9	:	800.	MM
TYPE	:	10	:	900.	MM
PIPE	:	11	:	1000.	MM
TYPE	:	12	:	1200.	MM
PIPE	:	13	:	1400.	MM
TYPE	:	14	:	1600.	MM
PIPE	:	15	:	1800.	MM
TYPE	:	16	:	2400.	MM

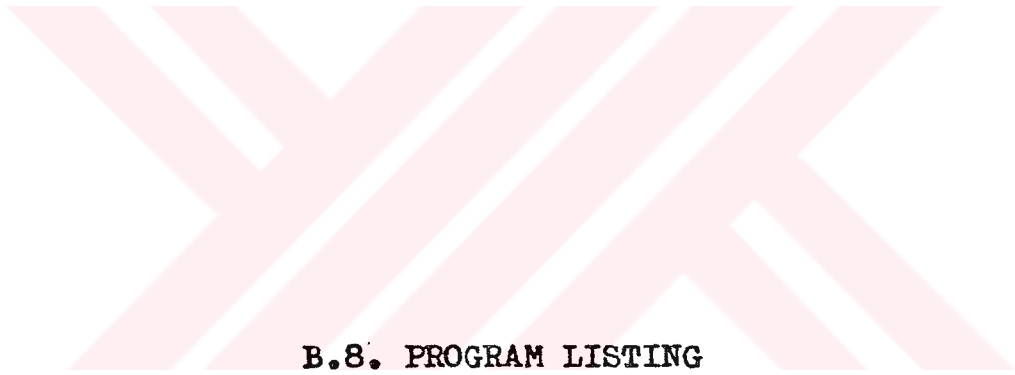
\*\*\*\*\*IN BOTH SEWERS AND COLLECTORS THE SAME ABOVE SECTIONS WILL BE USED\*\*\*\*\*

DESCRIPTION OF OUTPLT TITLE PARAMETERS

ITH : UPSTREAM NODE NUMBER  
 U : UPSTREAM NODE CONDITION  
 BLANK : UPSTREAM END OF A GUTTER OF MOST EXTREME INLET  
 I : INLET  
 M : MANHOLE  
 B : COLLECTOR JUNCTION  
 D : DOWNSTREAM NODE  
 Y : INLET  
 P : MANHOLE  
 T : TOTAL AREA DRAINAGE AT NODE ITH ( HA )  
 A : AREA DRAINAGE BY THE INLET JTH ( HA )  
 S : SLOPE OF SUBCAT ( M/M )  
 U : UPSTREAM NODE ELEVATION ( M )  
 D : DOWNSTREAM NODE ELEVATION ( M )  
 T : TRANSITION SECTION TYPE  
 Y : STAGNATION DISCHARGE OF SEWER OR COLLECTOR ( LT/SEC )  
 P : FULL DEPTH IN SEWER OR COLLECTOR ( M )  
 V : DESIGN FLOW RATE IN GUTTER FOR SMALL INTENSITY ( LT/SEC )  
 Y : PEAK FLOW RATE IN GUTTER FOR CRIP ( CM )  
 P : PEAK FLOW RATE INDEX FOR SUBCATCHMENT ( M/HR )  
 Y : ABSTRACT FACTOR OF SUBCATCHMENT  
 P : MANHOLE STRUCTURES ( CM )  
 Y : HEIGHT OF ADDITIONAL INLETS



ITEM	U	JTP	ICI	TAREA	AREA	ALEN	SLOFY	UFELEVI	DELEVI	UP	CCAN	TYPE	GDIS	QFUL	Y	V	TIM	GP	K	Y	P	K	P	H	Y	K	U	INC	U	
11	1	2	11	0.07	45.0	C	C5C	E75	CC	1876.28									7.97	2.3	127.	0.040								
11	1	3	11	0.04	45.0	C	C20C	E75	CC	1876.28									0.56	0.8	163.	0.060								
21	1	4	11																											
31	1	4	11																											
41	1	5	11	0.11	77.0			E76.2E	1863.54	1875.0E	1668.74	200	6.5	76.5	0.0C	1.1	6												0	
21	1	6	11	0.11	77.0	C	C6C	E76	28	1863.94									12.53	2.5	127.	0.040								
71	1	8	11	0.33	77.0	C	C20C	E76	28	1863.94									4.50	1.7	163.	0.060								
51	1	10	11	0.17	55.0	C	C20C	E70	7C	1859.94									2.30	2.0	163.	0.060								
61	1	5	11																											
81	1	5	11																											
101	1	5	11																											
51	1	11	11	0.72	45.0			E69.94	1863.72	1868.74	1667.52	200	28.0	43.9	0.13	1.3	12												0	
61	1	12	11	0.06	45.0	C	C10C	E65	54	1869.72									6.81	2.5	127.	0.040								
11	1	13	11	0.13	78.0	C	C5C	E75	CC	1869.72									14.81	2.5	127.	0.040								
11	1	14	11	0.11	78.0	C	C20C	E75	CC	1868.72									12.53	2.3	127.	0.040								
121	1	11	11																											
131	1	11	11																											
141	1	11	11																											
111	1	15	11	1.02	47.0	C	C7C	E66	72	1867.12									10.25	2.3	127.	0.040								0
141	1	16	11	0.09	47.0	C	C7C	E66	72	1867.12									19.36	2.3	127.	0.040								
171	1	18	11	0.17	73.0	C	C10	C42C	E77	11	1867.12								13.67	2.4	127.	0.040								
171	1	19	11	0.12	70.0	C	C21C	E77	11	1867.12																				
151	1	15	11																											
181	1	15	11																											
161	1	15	11																											
151	1	20	11	1.43	46.0			E67.12	1865.42	1853.82	1664.12	300	105.4	151.1	0.21	2.0	14												0	
211	1	22	11	0.17	78.0	C	C10	C42C	E71	48	1865.42								19.36	3.0	127.	0.040								
211	1	23	11	0.09	78.0	C	C10	C20C	E71	48	1865.42								10.25	2.4	127.	0.040								
151	1	24	11	0.09	46.0	C	C7C	E67	12	1865.42									10.25	2.7	127.	0.040								
241	1	20	11																											
221	1	20	11																											
231	1	20	11																											
201	1	25	11	1.75	46.0			E65.42	1862.85	1864.12	161.55	300	145.3	185.7	0.23	2.6	15												0	



**B.8. PROGRAM LISTING**







```

1.....2.....3.....4.....5.....6.....7.....8
SYCP
100 READ(P,110) (TYPEA(1,I),TYPEA(3,I),I=1,NCANAL)
110 FORMAT(1,6E5,C) GC TC 8C
DD I=1,NCANAL
WRITE(R,120) I,TYPEA(1,I),TYPEA(3,I)
120 * FORMAT(3CX,'CANAL TYPE =',I2,5X,'WIDTH: B =',F6.2,' METER',5X,
* 'HEIGHT: Y =',F6.2,' METER')
* TEMPE=TYPEA(3,I)*RATK
A=TYPEA(1,I)*TEMP
130 TYPEA(2,I)=(A/(TYPEA(1,I)+2*TEMP))**(2./3)*A
GO TO 30
140 READ(P,110) (TYPER(I),I=1,NPIPE)
IF(INSECA.EC.1) GO TO 16C
DO I=1,NPIPE
145 WRITE(R,150) I,TYPER(I)
150 * FORMAT(4CX,'PIPE TYPE =',I2,5X,'DIAMETER: D =',F5.0,' MM')
GO TO 17C
160 DRCP=C
170 CONTINUE
GUTRZ=GUTRN*0.375*(GUTRZ+1)**0.25/(0.5*GLTRZ)**0.625
Z=1/TRAP.GT.C READ(P,110) ((TYPEC(I,J),J=1,3),J=1,NTRAP)
IF(INSECB.NE.2) GC TC 22C
IF(INTRAP.LE.C.AND.NSECB.EC.2) GO TO 130
GO TO 195
130 WRITE(R,190)
190 * FORMAT(//,'X,120('),/10X,'ERROR : NUMBER OF STANDARD SECTIONS FO
R COLLECTORS HAS NOT BEEN FOUND IN INPUT DATA')
STOP
135 WRITE(P,200) TRAP,RAT
200 * FORMAT(//,'X,10('),/10X,'ONLY TRAPEZOIDAL SECTIONS WILL BE USED FOR
COLLECTOR',I2,'X,10('),/41X,'NUMBER OF STANDARD SECTIONS :',I3//41X,
* 'MAXIMUM DEPTH RATIO FOR TRAPEZOIDAL SECTIONS :',F6.3//,
* 41X,'MAXIMUM DEPTH RATIO FOR TRAPEZOIDAL SECTIONS :',F6.3//)
DO I=1,NTRAP
TYPEC(5,I)=TYPEC(1,I)+TYPEC(3,I)*RATT)*TYPEC(3,I)*RATT
TYPEC(4,I)=TYPEC(2,I)+TYPEC(5,I)**(2./3)
*+TYPEC(2,I)**2)**(2./3)

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MEITU 1121
MEITU 1122
MEITU 1123
MEITU 1124
MEITU 1125
MEITU 1126
MEITU 1127
MEITU 1128
MEITU 1129
MEITU 1130
MEITU 1131
MEITU 1132
MEITU 1133
MEITU 1134
MEITU 1135
MEITU 1136
MEITU 1137
MEITU 1138
MEITU 1139
MEITU 1140
MEITU 1141
MEITU 1142
MEITU 1143
MEITU 1144
MEITU 1145
MEITU 1146
MEITU 1147
MEITU 1148
MEITU 1149
MEITU 1150
MEITU 1151
MEITU 1152
MEITU 1153
MEITU 1154
MEITU 1155
MEITU 1156
MEITU 1157
MEITU 1158
MEITU 1159
MEITU 1160

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1.....2.....3.....4.....5.....6.....7.....8
927X,ITAREA : INLET//27X,M : MANHOLE//27X,P : COLLECTOR JUNCTION//,
920X,ALALEA : TOTAL AREA DRAINED AT NODE ITH (FA)//
WRITE(1,252)
*20X,ALALEA : AREA DRAINED BY THE INLET JTH (HA)//,
*20X,SLOPEY : LENGTH OF SUBCATCHMENT (M) //, (M/M) //, (M) //,
*20X,SLOPEY : SLOPE OF TOPOGRAPHIC ELEVATION (M) //,
*20X,UELEV : DOWNSTREAM OR COLLECTOR ELEVATION AT UPSTREAM END (M) //,
**20X,UELEV : ELEVATION OF SEWER OR COLLECTOR AT DOWNSTREAM END (M) //
**//,DOWNTYPE : DESIGN DISCHARGE OF SEWER OR COLLECTOR (LT/SEC) //,
**20X,UELEV : FULL CAPACITY OF SEWER OR COLLECTOR (LT/SEC) //,
**20X,UELEV : FLOW DEPTH IN SEWER OR COLLECTOR (M) //,
**20X,UELEV : PEAK FLOW RATE (M/GIT) //, OR COLLECTOR (M/SEC) //,
**20X,UELEV : PEAK FLOW RATE IN GUTTER IN SEWER OR COLLECTOR (LT/SEC) //,
**//,CPIK : YPIK : TIME IN GUTTER FOR SMALL INTENSITY (LT/SEC) //,
**20X,UELEV : PEAK FLOW INDEX FOR SUBCATCHMENT (CM) //,
**20X,UELEV : STRAINING FACTOR OF SUBCATCHMENT //,
**20X,UELEV : HEIGHT OF CHUTE STRUCTURES (CM) //,
**20X,UELEV : NUMBER OF ADDITIONAL INLETS //
WRITE(1,121('---'))
4  WRITE(1,15)
5  WRITE(1,17)
*  WRITE(1,7)
7  WRITE(1,7)
** UP NC
**  CCWN
**  ITH
WRITE(1,6)
6  WRITE(1,6)
PROGRAM S T C ANCE THE
C 300 READ(P,310,END=999) ITH,KP,JTH,KR,AREA,ALEN,AELEV,BELEV,PHY,AN,
* SLOPEY,ALENY,LP,NCCI,NCCJ
310 WRITE(2(14,A1),8PF6,C,T65,314)
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METU 240



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.....1.....2.....3.....4.....5.....6.....7.....8
IF(AELEV-BELEV) 311,315,313
IF(ALEN.EQ.0.) GC TC 313
315 WRITE(R,312) ITH,KP,JTH,KR,AREA,ALEN,AELEV,BELEV,PFY,AN,SLCFY,
311 *ALENY,LP,NCDI,123(*,)/ICX,ERROR : NON POSITIVE SLOPE FOR THE FOLL
312 *FORMING DATA CARE//ICX,2(I4,A1), 8F9.4,5X,316)
STOP
313 CONTINUE
IF(KP.EQ.0) GO TO 340
IF(KP.EQ.1) GO TO 320
IF(KP.EQ.2) GO TO 330
IF(KP.EQ.3) GO TO 320
IF(KP.EQ.4) GO TO 320
IF(KP.EQ.5) GO TO 320
IF(KP.EQ.6) GO TO 320
IF(KP.EQ.7) GO TO 320
IF(KP.EQ.8) GO TO 320
IF(KP.EQ.9) GO TO 320
IF(KR.EQ.0) GO TO 530
IF(KR.EQ.1) GO TO 900
320 WRITE(R,315,123(*,)/ICX,ERROR : BOUNDARY CCNDITION AT DCWASTREA
335 *FORMAT(//IX,123(*,)/ICX,ERROR : BOUNDARY CCNDITION AT DCWASTREA
STOP
C-----COMPLATION OF EACH CARD DATA STARTS FROM HERE ACCORDING TO
C THE TRANSFER OF DATA CARD
336 DO 337 I=1,JK
337 CONTINUE
338 DO 339 J=1,IJK
339 HYDR(I,J)=C
ITEMP(I)=999
DO 350 I=1,JK
340 IF(LOGIC(I).EQ.0) GC TC 360
350 CONTINUE
GO TO 358
ITEMP(I)=JTH
TEMPC(I)=AREA
LOGIC(I)=1
SLOPE=(AELEV-BELEV)/ALEN
CALL HYDCAL(I,AHYD,NNN)

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METU 241
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METU 279
METU 280

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.....1.....2.....3.....4.....5.....6.....7.....8
APIK=GPIK
BPIK=YPIK
DO 370 J=1,IJK
FYDA(I,J)=AHYD(J)
AHYD(I,J)=C
CALL HYDCG,ALIDES,CHYE,KKK)
CALL ROUTE
DJ 400 J=1,IJK
HYDB(I,J)=CHYD(J)
DHYD(J)=C
CHYD(J)=C
IF(YPMAX.LT.YPIK.OR.SMAX.LT.CPIK) GO TO 410
TEMP(I)=RELIV-DFCP
WRITE(R,5)
WRITE(R,405) ITH,KF,JTH,KP,AREA,ALEN,SLOPY,AELEV,BELEV,CPIK,YPIK,
*PHY,AN
405 FOR MAT(1H+,2(I5,IX,4I),8X,F6.2,F6.1,F7.4,2F7.2,48X,F6.2,F5.1,F4.C,
*F6.3,F6.6)
WRITE(R,6)
IF(KR.EQ.EEE) CC TC 441
GO TO 300
CALL RATIO
410 N=N+1
420 ALEN=ALEN/N
AREA=AREA/N
CALL HYCCAL(1,AHYD,ANN)
IF(YPMAX.LT.YPIK.OR.SMAX.LT.CPIK) GO TO 430
IF(NEQ.440)
GO TO 440
430 ALEN=ALEN*N
AREA=AREA*N
GO TO 420
440 AREA=AREA*N
ALCN=ALEN*N
N=N-1
WRITE(R,5)
WRITE(R,405) ITH,KF,JTH,KR,AREA,ALEN,SLOPY,AELEV,BELEV,APIK,BPIK,
*PHY,AN
WRITE(R,6)
IF(KR.EQ.EEE) CC TC 441
.....1.....2.....3.....4.....5.....6.....7.....8

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METU 231
METU 282
METU 283
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METU 319
METU 320

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.....1.....2.....3.....4.....5.....6.....7.....8

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441 GO TO 300
442 LI=I
443 DO I=1,J,K
444 IF(JTH.EG.YTEMP(I).ANC.LI.NE.I) GO TO 143
445 CJN TO 144
446 DO I=1,IJK
447 FVD(I,J)=HYDR(I,J)+FYCB(LI,J)
448 TEMP(I,J)=TEMPC(I)+AREA
449 LOGIC(LI)=C
450 YTEMP(LI)=-9595
451 TEMP(LI)=C
452 GO TO 300
453 I=I
454 DO I=1,IJK
455 FVD(I,J)=HYDR(LI,J)
456 GO TO 300
457 CALL HYCAL(ICES,CFYC,KKK)
458 NJ=NN+1
459 BELEV=AELEV-SLOPE*ALEN
460 WRITE(R,5)
461 *PHY,AN
462 WRITE(R,6)
463 DO J=1,NNN
464 BHYD(J)=AHYD(J)
465 BPA=BELEV-DRCR
466 CALL ROUTE
467 LE=C
468 NN=10
469 K=1,N
470 NN=NN+1
471 NN=NN+1
472 IF(K.EG.N) N=JTH
473 IF(K.EG.N) CCC=KP
474 AELEV=BELEV
475 AELEV=AELEV-SLOPE*ALEN
476 CALL DESIGN(BHYD,VMIN,VMAX,NSECA,NK,NN)
477 CALL TCDPLAM
478 CALL SIMPLAM

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.....1.....2.....3.....4.....5.....6.....7.....8

.....1.....2.....3.....4.....5.....6.....7.....8

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AREA=AREA*K
WRITE(R,5) NK,CCC,NN,CCC,TAREA,AREA,ALEN,SLCFY,AELEV,BELEV,UP,
WRITE(R,8) CUL,Y,V,TIME,CPIK,YPIK,PHY,AN,NCHUTE
*DOWNL(IH+,2(I5,IX,AL)),F8.2,F6.1,F7.4,4F7.2,15,2F7.1,F5.2,F6.
470 *1,14,F6.2,F5.1,2F5.2,I4)
WRITE(R,6)
IF(L,LE,LMIN) GC TC 521
GO TO 471
521 ITHS(NMN)=NK
ITHS(NMN)=NN
NMN=NMN+I
NPA=DCWNA
471 DO 450 J=1,NN
DO BHYD(J)=RHVD(J)+AHVD(J)
500 CALL INUTE
510 CCC=366
NN=NN+1
DO 520 J=1,IJK
HYD(I,J)=RHVD(J)
HYD(I,J)=EHVD(J)
520 JTEMP(I,J)=EHVD(J)
JTEMP(I)=LCCWNA
GO TO 300
530 IF(NMEC,NE.2) GC TC 336
DO 540 I=1,IJK
IF(ITH,EG,ITEMF(I)) GO TO 550
540 GO TO 339
550 DO 560 J=1,IJK
DHVD(J)=HYD(I,J)
BHYD(J)=HYD(I,J)
EHVD(J)=HYD(I,J)
HYD(I,J)=0.
560 HYD(I,J)=0.
HYD(I,J)=399
IAAA=ITEMF(I)

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METU 361
METU 362
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METU 370
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METU 398
METU 399
METU 400

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.....1.....2.....3.....4.....5.....6.....7.....8

.....1.....2.....3.....4.....5.....6.....7.....8

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SLOPE=(AELEV-BELEV)/ALEN
UPA=TEMP(I)
L=JTEMP(I)=0
LOGGIC(I)=C
YTEMP(I)=-5959
TEMPC(I)=0
CALL HYDCAL(I,AHYD,NNN)
CALLY MAX,LT,YPIK,CR,CMAX,LT,QPIK) GO TO 570
IF(LT,DESIGN(BHYD,VMIN,VMAX,NSECA,ITH,JTH)
WRITE(I,5)
WRITE(I,67C) ITH,KP,JTF,KR,AAAA,AREA,ALEN,SLCFY,AELEV,BELEV,UP,
*DOWN,LE,BIG,QFUL,Y,V,TIME,GPIK,YPIK,PHY,AN,NCH,IE
IF(L,LE,LMIN) CC TC 611
WRITE(I,6)
IF(L,LE,LMIN) CC TC 611
CALL SIMCLAM
CALL HYDCAL(IDES,CHYC,KKK)
CALL RCTE
CT=561
DO 561 I=1,JK
IF(JTH,EG,ITEMF(I)) GO TO 562
CONTINUE
I=LT
DO 610 I,J=1,IJK
HYDCAL(I,J)=BHYD(J)
HYDB(I,J)=CHYC(J)
HYCC(I,J)=EHYC(J)
HYOC(I,J)=DHYD(J)+EHYC(J)
BHYD(I,J)=C
DHYD(I,J)=C
EHYD(I,J)=C,JTH
JTEMP(I)=LOWNA
JTEMPB(I)=AAAA+AREA
LOGGIC(I)=1
GO TO 30C
GD TO 30C
JTHS(NMN)=JTH
JTHS(NMN)=JTH

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METU 401
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NMN=NMN+1
GO TO 564
DO 600 J=1, IJK
HYDCA(I, J)=EHYC(J)
HYDCB(I, J)=HYCB(J)
HYDC(I, J)=EHYD(J)+FYCC(I, J)
AHYD(I, J)=C
CHYD(I, J)=C
DHYD(I, J)=C
EHYD(I, J)=C
TEMPC(I)=AAA+TEMP(I)+AREA
TEMP(I)=LT.L) JTEMP(I)=L
GO TO 300
CALL RATIO
NEN=1
AREA=ALEN/N
AREA=AREA/N
CALL HYDCAL(I, AHYD, NNN)
IF (YMAX, YPIK, AND, CMAX, GT, CPIK) GO TO 580
ALEN=ALEN*N
AREA=AREA*N
GO TO 575
530 BELEV=AELEV-SLCP*ALEN
NK=INTH
DO 530 K=1, N
TAREA=AREA*(K-1)+AAA
NN=NN+1
IF (K, DESIGN(BHYD, VMIN, VMAX, NSECA, NK, NN)
CALL CORR, 5)
WRITE(R, 470) NK, CCC, NN, CCC, TAREA, AREA, ALEN, SLCPFY, AELEV, BELEV, UP,
*DOWN, L, BIG, CFUL, Y, V, TIME, CPIK, PHY, AA, NCHOTE
WRITE(L, 581)
IF (L, LE, LMIN) GO TO 591
GO TO 581
ITHS(NMN)=NK
JTHS(NMN)=NN
NMN=NMN+1
AELEV=BELEV

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.....1.....2.....3.....4.....5.....6.....7.....8

.....1.....2.....3.....4.....5.....6.....7.....8

BELEV=AELEV-SLOPE\*ALEN  
UPA=CCWNA  
NK=NN J=1,NNN  
DO 551 J=1,NNN  
BHYD(J)=BHM  
CALL YCPPLAM  
CALL SIMULM  
CALL HYDCAL(IDCS,CFYD,KKK)  
CALL ROUTE  
CONTINUE  
CONTINUE  
AREA=AREA\*N  
GO TO 565  
GO 310 J=1,JK  
IF(I,TEMP(I),EQ,ITH) GO TO 820  
CONTINUE  
GO TO 830 J=1,JK  
DO 830 MPR(J),EQ,JTH) GO TO 840  
IF(I,TEMP(I),EQ,JTH) GO TO 840  
CONTINUE  
GO TO 850  
DO 360 K=1,IJK  
HYDA(J,K)=HYCA(I,K)+FYCA(J,K)  
HYDB(J,K)=HYCB(I,K)+HYCB(J,K)  
HYDC(J,K)=HYCC(I,K)+FYCC(J,K)  
HYDB(I,K)=C.  
HYDC(I,K)=C.  
LOSIC(I)=C  
LOTEMP(I)=TEMPC(J)+TEMPC(I)  
TEMPC(I)=0  
JTEMP(I)=0  
TEMP(I)=0  
GO TO 851 JTH  
ITEMP(I)=JTH  
WRITE(R,2) ITH,KF,JTH,KR  
2 FORMAT(1F+,2(I,IX,AI))  
WRITE(R,6)  
GO TO 300



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542 ITEMP(I)=JTH
    JTEMP(I)=L
    TEMPB(I)=DCWNA
    TEMPC(I)=AAAA+AREA
    LOGIC(I)=1
    DO 945 J=1,IJK
    HYDA(I,J)=BHYD(J)
    HYDC(I,J)=EHYD(J)
    BHYP(I,J)=C
    IF(KR.EQ.EEE) GO TO 950
    GO TO 900
546 ITHS(MN)=JTH
    JTHS(MN)=JTH
    MN=MN+1
    GO TO 921
550 JTEMP(I)=0
    DO 960 J=1,IJK
560 HYD(I,J)=EHYD(J)
    GO TO 930
570 DO 980 J=1,IJK
    HYDA(K,J)=BHYD(J)
    HYDC(K,J)=EHYD(J)
580 TEMPC(K)=AAAA+TEMP(I)+AREA
    IF(TEMPB(K).GT.DCWNA) TEMPB(K)=L
    IF(JTEMP(K).LT.L) JTEMP(K)=L
    IF(KR.EQ.EEE) GO TO 985
    GO TO 900
585 JTEMP(K)=C
    DO 986 J=1,IJK
586 HYD(X,J)=EHYD(J)
590 GO TO 900
1000 LOGIC(M)=1,JK
1001 CONTINUE
    GO TO 8382
1001 LOGIC(M)=1
    DO 1002 MM=1,JK
1002 IF(LOGIC(MM).EQ.0) GO TO 1003
    CONTINUE
.....1.....2.....3.....4.....5.....6.....7.....8

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METU 561
METU 562
METU 563
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METU 599
METU 600

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METU 636  
METU 637  
METU 638  
METU 639  
METU 640

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GO 1004 J=1,IJK
HYDB(M,J)=CHYD(J)/2.
DHVDB(J)=C
ITEMP(M)=NCDI
ITEMP(MM)=I
LOGIC(M)=I
GO 1006 M=1,JK
DO LOGIC(M).EQ.0 GC TC 1050
IF (LOGIC(M).EQ.0) GC TC 1050
CONTINUE
GO 1008 M=1,JK
DO LOGIC(M).EQ.0 GC TC 1095
IF (LOGIC(M).EQ.0) GC TC 1095
CONTINUE
ITEMP(M)=NCDI
ITEMP(M)=1,JK
HYDB(M,J)=CHYD(J)
DHVDB(J)=C
LOGIC(M)=I
GO 1210 M=1,JK
DO LOGIC(M).EQ.0 GC TC 1220
IF (LOGIC(M).EQ.0) GC TC 1220
CONTINUE
READ(1,230) (HYD(I,J),J=1,NODJ)
FORMAT(9F10.0)
ITEMP(I)=JTH
ITEMP(I)=I
LOGIC(I)=I
IF (ITEMP(I).EQ.0) GC TC 851
WRITE(R,5) JTH,INFLCW HYDROGRAPH AT NODE',I5,' IN LT/SEC'/(5X,15F8)
FORMAT(//10X,15F8)
* I)
WRITE(R,6)
GO 1001
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.....1.....2.....3.....4.....5.....6.....7.....8

.....1.....2.....3.....4.....5.....6.....7.....8

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2000 DO 2010 J=1,JK
      IF (JTH.EG. ITEMP(I)) GO TO 2020
2010 CONTINUE
2020 DO 2030 J=1,IJK
      FHYD(J)=FHYD(I,J)
2030 HPA=ALELEV-CRCP
      UAAA=ATEMPC(I)
      LTEMP(I)=-9999
      ITEMPC(I)=C
      LOGIC(I)=C
      IF (LPA.NE.0) WRITE(R,5) ITH,(FHYD(J),J=1,IJK)
      IF (LPA.NE.0) WRITE(R,6)
      CALL DESIGN(FHYD,C,VV,AXE,NSECB,ITH,JTH)
      WRITE(R,5) ITH,KF,JTH,KR,AAAA,ALEN,ALELEV,BELEV,UP,DOWN,L,BIG,QFUL,
      *Y,V,YE(R,6) NCHUTE
      DO 2040 I=1,IJK
      IF (JTH.EG. ITEMP(I)) GO TO 2060
2040 CONTINUE
2050 I=1,JK
      IF (LOGIC(I).EQ.0) GO TO 2060
2060 CONTINUE
      ITEMP(I)=JTH
      KTEMP(I)=LAAAA+AREA
      TEMPA(I)=BELEV
      LOGIC(I)=1
      DO 2070 J=1,IJK
      FHYD(I,J)=FHYD(J)
2070 GO TO 30C
2080 DO 2090 J=1,IJK
      FHYD(I,J)=FHYD(I,J)+FHYD(JJ)
2090 TEMPC(I)=AAAA+TEMPC(I)+AREA
      GO TO 30C
3888 WRITE(R,9950)
3990 FORMAT(//IX,130(' '))/10X,'ERROR : INSUFFICIENT DIMENSION OF ARRAY

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MEIU 641  
 MEIU 642  
 MEIU 643  
 MEIU 644  
 MEIU 645  
 MEIU 646  
 MEIU 647  
 MEIU 648  
 MEIU 649  
 MEIU 650  
 MEIU 651  
 MEIU 652  
 MEIU 653  
 MEIU 654  
 MEIU 655  
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 MEIU 660  
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 MEIU 664  
 MEIU 665  
 MEIU 666  
 MEIU 667  
 MEIU 668  
 MEIU 669  
 MEIU 670  
 MEIU 671  
 MEIU 672  
 MEIU 673  
 MEIU 674  
 MEIU 675  
 MEIU 676  
 MEIU 677  
 MEIU 678  
 MEIU 680

.....1.....2.....3.....4.....5.....6.....7.....8

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1.....2.....3.....4.....5.....6.....7.....8
* LOGIC(1)
  GO TO 5555
8899 WRITE(R,2899) ITH
8891 FORMAT(/,1X,130('**')/10X,'ERROR : UPSTREAM NCEE',I5,' CAN NOT BE
3599 *FOUND IN ARRAY(S)')
      NMN=NMN-1
      IF(NMN.GT.0) WRITE(R,8) (I1HS(I),I=1,NMN)
      B FORMAT(/,10X,'SEWERS BETWEEN THE FOLLOWING ADDRES HAVE SMALL SEC
      TIONS THEN THE SPECIFIED',/10X,'A NEW RUN MAY BE NECESSARY BY RE
      *MOVING, CORRESPONDING INLETS,/10X,'NODES: FROM TO',/117X,I4,2X,
      <I4>)
      WRITE(R,5555)
      FORMAT(/,10X,'POINT(S) OF DISPOSAL :',/)
5555 DO 5557 I=1,JK
      IF(ITEMP(I).GT.0) WRITE(R,5556) ITEMP(I)
5556 FORMAT(25X,I5)
5557 CONTINUE
      STOP
C-----END OF THE MAIN PROGRAM
C-----END
C-----SUBPROGRAM TCPLAN DETERMINES THE DISCHARGE INTERCEPTED
C-----AND THE CARRY-OVER FROM AN INLET
      SUBROUTINE TCPLAN
      COMMON/LAMDA/QFUL,P,R
      COMMON/SICMA/IJK
      COMMON/TAL/DHYE(250)
      COMMON/RFC/EHYE(250)
      DO 1000 J=1,IJK
      DHYD(J)=EHCYD(J)+EHYD(J)-GEUL
      IF(DHYD(J).LT.0.) GO TO 2000
      EHYD(J)=DHYD(J)
      GO TO 1000
      2000 DHYD(J)=EHCYD(J)+QFUL
      1000 DHYD(J)=0.
      CONTINUE
      RETURN
      END

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METU 681
METU 682
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METU 684
METU 685
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METU 688
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METU 709
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METU 711
METU 712
METU 713
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METU 715
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METU 717
METU 718
METU 719
METU 720

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.....1.....2.....3.....4.....5.....6.....7.....8

-----END OF THE SUBPROGRAM ICFLAM

SUBPROGRAM HYDICAL DETERMINES THE INLET HYDROGRAPHS FOR SMALL  
RETURN PERIODS AND SURFACE HYDROGRAPHS FOR LARGE RETURN PERIODS

SUBROUTINE HYDICAL(ICES,AHYD,NNN)  
DIMENSION AHYD(250)  
COMMON/GAMA/ALEN,DELT  
COMMON/CHY/ALENY,SLOPY,PHY,AN,TCA,TDB,AINTA,AINTB,AREA  
COMMON/BEFA/GCTR,YPJK  
COMMON/BEFA/GCTR,YPJK  
COMMON/SIGMA/IJ  
TC=6.92/AINTA\*\*C.4\*((AN\*ALENY)\*\*2./SLOPY)\*\*C.3  
IF(ICES.NE.1) GO TO 2100  
CP=AREA\*(AINTA-PHY)/360

OS=QP  
TD=TDATA  
I=1

2010 Q=CP  
I=I+1  
Y=(Q/5\*\*2)\*Y\*\*2.  
AVH=C/AEN/VH/60  
TH=ALC+TH  
TA=IC+TH  
IF(TD.GE.TA) GC TO 2040  
CP=TD/TA\*CS  
IF(I.EQ.2) GO TO 2010

2015 CP=CP\*(2\*TA-ID)\*DELT  
Q1=CP/ID\*DELT  
NN=TD/DELT+0.5  
NNN=2\*TA/DELT  
IF(NNN.GT.IJK) NNN=IJK

2020 DD=2\*Q1  
AHYD(I)=CI\*Y  
NN=NN+1  
DA=30\*Q1  
AHYD(I)=CP-22\*(I-NN+1)

2030 G) TT 2070

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MEIU 726  
MEIU 727  
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MEIU 736  
MEIU 737  
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MEIU 740  
MEIU 741  
MEIU 742  
MEIU 743  
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MEIU 748  
MEIU 749  
MEIU 750  
MEIU 751  
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MEIU 758  
MEIU 759  
MEIU 760

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METU 799  
METU 800

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2040 N=TD/CELLI+1.01
      NN=TA/CELLT
      NNN=N+NN
      IF(NNN.GT.IJK) NNN=IJK
      GP=CP*1000
      C=GP/TA*CELLT
      DO 2050 I=1,NN
      AHYD(I)=C*I
2050 AHYD(NNN-I)=AHYD(I)
      NN=NN+I
      N=NNN-NN
      DO 2060 I=NN,N
      AHYD(I)=CP
2060 IF(I.DES.NE.1) RETURN
2070 IF(IY=CP
      YPIK=(GP/1000/SCRT(SLCFE))*0.375*GUTRZ*100
      RETURN
2100 TD=TD+R
      TA=6.92/AINTB**C.4*((AA*ALENY)**2./SLOPY)**C.3
      CP=AREA/IDES*(AINTB-PHY)/360
      IF(TD.CE.TA) GC TC 2040
      GP=CP*TD/TA
      GO TO 2015
      END OF THE SUBPROGRAM FYCCAL
C-----
C-----
C-----
SUBPROGRAM RATIO DETERMINES THE REQUIRED NUMBER OF INLETS BETWEEN
TMC NEEDS TO KEEP GUTTER DISCHARGE AND FLOW DEPTH BELOW
THE SPECIFIED LIMITS
SUBROUTINE RATIO
COMMON/ALFA/CP, YPIK
COMMON/CRA/CMAX, YMAX, N
RATA=(YMAX/YPIK)**(5./3)
RATB=(YMAX/CP)
IF(RATA.GT.RATC) RATA=RATB
RETURN
END
C-----
END OF THE SUBPROGRAM RATIO
C-----

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.....1.....2.....3.....4.....5.....6.....7.....8

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.....1.....2.....3.....4.....5.....6.....7.....8
C-----SUBPROGRAM ROUTE RCTES THE GUTTER HYDROCGFAFF ICES TIMES BY
C-----ADDING HYDROGRAPH OF LARGE RETURN PERIOD EACH TIME
SUBROUTINE RCTUTE
DIMENSION CHYD(250)
COMMON/CRC/ YDES, ANA, CHYD
COMMON/TAU/ DHYD(250)
COMMON/BETA/ GUTRZ, Z, SLCPE
COMMON/SIGMA/ I, K
COMMON/GAMA/ ALFN, DELT
DO 480 M=1, IDES
DO 470 J=1, NAN
DHYD(J)=CHYD(J)
DHYD(I)=2* IJK
IF(DHYD(I).GT.G) G=CHYD(I)
CONTINUE
Y=(Q/1000C/SQRT(SLOPE)**C.375*GUTRZ
A=0.572*Y**2
V=G/1000./A*.60
IT=ALFN/ICES/V/DELT+1
K=IJK-IT
IF(K.LT.1) K=1
DO 2000 I=1, K
DHYD(IJK-I+1)=CHYD(K-I+1)
2010 DO 2010 I=1, IT
DHYD(I)=C.
CONTINUE
480 RETURN
END OF THE SUBPROGRAM ROUTE
C-----SUBPROGRAM DESIGN DETERMINES THE SECTIONS OF SEWERS AND COLLECTORS
C-----ACCORDING TO THE PEAK DISCHARGES OF HYDROGRAPHS. SUBPROGRAM ALSO
C-----ROUTINES THE HYDROGRAPHS OF SEWERS FOR SMALL RETURN PERIOD AND OF
C-----COLLECTORS FOR LARGE RETURN PERIOD
SUBROUTINE DESIGN
INTEGER R, CHYD(250)
DIMENSION BETA, CHYD(250)
COMMON/TETA/ LPA, DOWNA, PIPE, CANAL, L, TYPEA(4,20), IJKL, IRCUTE, ISTEP
.....1.....2.....3.....4.....5.....6.....7.....8

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803 METU
804 METU
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809 METU
810 METU
811 METU
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814 METU
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840 METU

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COMMON/CDE/TYPID(20),TYPEC(5,20),AELEV,BELEV,DFCP,NPIPE,NCANAL,
*INTRAP,TRAPA,TIME,BIG,Y,NART,NCHUTE,UP,DOWN,V
COMMON/LAMDA/QF,P,R
COMMON/SIGMA/IJK
COMMON/GAMA/ALEN,DELT
NCHUTE=0
YT=0
QC=0
ARA=DELT*30/ALEN
BIG=BHYD(1)
KK=1
DO 1000 I=2,IJK
VF(BHYS(I)).GT.EIG) KK=I
BIG=CHYE(KK)
CONTINUE
BIG=BIG/1000.
TIME=KK*DELT
SLOPE=(UFA-BELEV+DFCF)/ALEN
IF(NSLC(EG.1)) GC TO 1030
IF(NSLC(EG.2)) GC TO 1000
D=1.548*(PIPEN+BIG/SLOPE**0.5)**0.375 *1000.
DO 1020 I=1,NPIPE
IF(D.LE. TYPE(I)) GC TO 1060
CONTINUE
WRITE(R,1040) I,I,J,J
FORMAT(//IX,130(//IX,10X,'ERROR: STANDARD DIAMETERS ARE NOT BIG
1040 *ENOUGH TO DESIGN THE SEWER BETWEEN THE NODES',I5,'TH AND',I5,'TH')
WRITE(R,1) BIG,SLOPE,D,V
FORMAT(4F10.4)
STOP
IF((I+II).GT.NPIPE) GC TO 1030
DETYPEB(I+II)
IF(L.GT.E) D=L
AF=3.141553*(D/1000)**2/4
OR=816/GE
DR=0.67333*CR+C.22777E
TH=2*ARCCOS(1-2.*CR)
AR=(TH-SIN(TH))/6.282185

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.....1.....2.....3.....4.....5.....6.....7.....8

C



.....1.....2.....3.....4.....5.....6.....7.....8

MEIU 881  
MEIU 882  
MEIU 883  
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MEIU 885  
MEIU 886  
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MEIU 888  
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MEIU 919  
MEIU 920

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V=BIG/AR/AF
I=I+1
IF(V.GT.VMAX) AND (I.LE.NART) GO TO 1050
IF(V.GT.VMAX) CC TC 21CC
BIG=BIG*1000
Y=D*DR/1000
DOWNA=BELEV-DRCP
DOWN=DCMNA-D/1000.
UP=UPA-D/1000.
L=D
IF (IRCTE.NE.0) GO TC 2020
GO TO 1030
AR=BIG*CANALN/SCRT(SLOPE)
DO 1140 I=1,NCANAL
IF(AR.LT.TYPA(2,I)) GC TC 1150
CONTINUE
GO TO 1030
IF(L.LE.NCANAL.AND.L.GT.I) I=L
M=I+1
IF(M.GT.NCANAL) GO TC 1030
IF=TYPEA(2,M)*SCRT(SLOPE)/CANALN
B=TYPEA(1,M)
CALL YNCRM(YA,EIG,CANALN,SLOPE,B,0.)
Y=YN
A=Y*B
I=I+1
IF(V.GT.VMAX) AND (I.LE.NART) GO TO 1160
V=BIG/A
IF(V.GT.VMAX) CC TC 22CC
BIG=BIG*1000
DOWNA=BELEV-DRCP
DOWN=DCMNA-TYPEA(3,M)
UP=UPA-TYPEA(3,M)
L=M
IF (IRCTE.NE.0) GO TC 7030
IT=ALEN/V/DEL/60+1
K=IJK-I
IF(K.LT.1) K=1
DO 2000 M=1,K
BHYD(IJK-M+1)=BHYD(K-M+1)

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1130  
1140  
1150  
1160  
1165  
1590  
2000

.....1.....2.....3.....4.....5.....6.....7.....8

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.....1.....2.....3.....4.....5.....6.....7.....8
2010 DO 2010 M=L,IT
2015 BHYD(M)=C
2020 QF=QF*1000
2025 A=0
2030 DO 2023 J=1,IJKL
2035 IF(BHYD(J))=C.C.C.AND.EFYE(J+1).EQ.0.0.AND.CC.LT.C.0001)GO TO 5145
2040 XX=(BHYD(J+1))-BHYD(J)/ISTEP/2000
2045 DO 20 I=1,ISTEP
2050 DELTAP=ARAP/ISTEP*(YY+XX-GC)
2055 AR=AP+DELTAP
2060 IF(AP.LT.C.) AF=0.
2065 AR=AP/AF
2070 QR=1.C/37725*AR**1.388456
2075 IF(AR.GT.0.26)GR=1.C/5165*AR**1.418482
2080 CCB=CF*GR
2085 DELTA=ARA/ISTEP*2*(YY+XX-GCB)
2090 A=A+DELTA
2095 IF(A.LT.C.) A=C.
2100 AR=A/AF
2105 QR=1.C/37725*AR**1.388456
2110 IF(AR.GT.0.26)GR=1.C/5165*AR**1.418482
2115 CC=GR*CF
2120 YY=YY+2*XX
2125 CONTINUE
2130 GHYD(J+1)=GC*1000
2135 GJ TO 2023
2140 GHYD(J+1)=0.
2145 CONTINUE
2150 GHYD(I)=C.
2155 DO 5160 J=1,IJK
2160 GO TO 2015
2165 WA=BIC/VMAX
2170 D=1123.373*SGRT(WA)
2175 DD 211) K=1,NPIDE
2180 IF(D.LE.1)PER(I) CC TC 2160
2185 CONTINUE
2190 GO TO 1030
.....1.....2.....3.....4.....5.....6.....7.....8

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METU 921
METU 922
METU 923
METU 924
METU 925
METU 926
METU 927
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METU 956
METU 957
METU 958
METU 959
METU 960

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.....1.....2.....3.....4.....5.....6.....7.....8

MEIU 961  
MEIU 962  
MEIU 963  
MEIU 964  
MEIU 965  
MEIU 966  
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MEIU 978  
MEIU 979  
MEIU 980  
MEIU 981  
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MEIU 995  
MEIU 996  
MEIU 997  
MEIU 998  
MEIU 999  
MEIU 1000

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2160 DD=9/2000
ASLOPE=(BIG*PIFEN/DD**(.8/.3)) **2*9.2553124
NCHUTE=A*LEN*(SLOPE-ASLOPE)*100.
SLOPE=ASLOPE
GO TO 1080C
2200 WA=BIG/VMAX
DO 2210 K=1,NCANAL
IF(WA.LE.*TYPEA(4,I)) GC TC 2260
CONTINUE
2210 GO TO 1030
ASLOPE=(BIG*CANALN/TYPEA(2,I))**2.
NCHUTE=A*LEN*(SLOPE-ASLOPE)*100.
SLOPE=ASLOPE
GO TO 1165
3000 AR=BIG*TRAPN/SGRT(SLOPE)
DO 3140 I=1,NTRAP
IF(AR.LT.*TYPEA(4,I)) GC TC 3160
CONTINUE
3140 GO TO 1030
3160 M=I+1
IF(M.GT.NTRAP) GO TO 1030
IF(*TYPEA(4,M))*SGRT(SLOPE)/TRAPN
3165 B=*TYPEA(1,I)
7=*TYPEA(2,I)
CALL YNCRM(YN,DIG,TRAPN,SLOPE,B,Z)
Y=YN
A=(TYPEA(1,I)+TYPEA(2,I))*Y
V=BIG/A
II=I+1
IF(V.CT.VMAX.AAC.II.LE.NART) GO TO 1160
IF(V.CT.VMAX) CC TC 4000
BIC=BIG*1000
DOWN=SCWNA-TYPEA(3,M)
L=M
IF(IRCUTE.NE.0) GC TC 8130
GO TO 1030C
4000 WA=BIG/VMAX
DO 4010 I=M,NTRAP
IF(WA.LE.*TYPEA(5,I)) GC TC 4020

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.....1.....2.....3.....4.....5.....6.....7.....8

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.....1.....2.....3.....4.....5.....6.....7.....8
4010 CONTINUE
4020 G1 TO 1030
ASLOPE=(PIG*TRAPN/TYPEC(4,I))*2
NCHUTE=ALEN*(SLOPE-ASLCP)*100.
SLOPE=ASLCP
MEI TO 3165
7030 A=0
DO 7160 J=1,IJKL C,ANC,BHYD(J+1),EQ,0,0,AND,CC,LT,C,CCO1)GC TC 7140
IF(BHYD(J),C,)-RHYD(J))/ISTEP/2)00
XX=(BHYD(J))/ICCC
YY=31 I=1,ISIEF
DELTA=ARAI/ISTEP*(YY+XX-CC)
AP=A+DELTA
IF(AP,LT,C) AF=0.
OCB=SQRT(SLOPE)/CANALN*AP*(5./3)*(B/(B**2+2*AP))**(2./3)
DELTA=AP/ISTEP*2*(YY+XX-CCB)
A=A+DELTA
IF(A,LT,C) A=C
QC=SQRT(SLOPE)/CANALN*A*(5./3)*(B/(B**2+2*A))**(2./3)
YY=YY+2*XX
21 CONTINUE)=CC*ICCC
GO TO 7160
7140 GHYD(J+1)=C.
7160 CONTINUE
8130 A=0.
DO 8160 J=1,IJVL
IF(BHYD(J),C,)-RHYD(J+1),EQ,0,0,AND,CC,LT,0.0001)GO TO 8140
XX=(BHYD(J))/ICCC
YY=31 I=1,ISIEF
DELTA=ARAI/ISTEP*(YY+XX-CC)
AP=A+DELTA
IF(AP,LT,C) AF=C
OCB=SQRT(SLOPE)/TRAPN*AP*(5./3)*(1/(B+(-B+SQRT(B**2+4*AP*Z))/Z))*
*SQRT(1+Z**2)
DELTA=ARAI/ISTEP*2*(YY+XX-CCB)
.....1.....2.....3.....4.....5.....6.....7.....8

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MEI10001
MEI10002
MEI10003
MEI10004
MEI10005
MEI10006
MEI10007
MEI10008
MEI10009
MEI10010
MEI10011
MEI10012
MEI10013
MEI10014
MEI10015
MEI10016
MEI10017
MEI10018
MEI10019
MEI10020
MEI10021
MEI10022
MEI10023
MEI10024
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MEI10026
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MEI10028
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MEI10030
MEI10031
MEI10032
MEI10033
MEI10034
MEI10035
MEI10036
MEI10037
MEI10038
MEI10039
MEI10040

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1.....2.....3.....4.....5.....6.....7.....8
A=A+DELTA
IF(A.LT.C.) A=C
QC=SQRT(SLOPE)/TRAFN*A**(5./3)*(1/(B+(-B+SQRT(B**2+4*A*Z)))/Z)*
*SQRT(1+7**2)
YY=YY+2*XX
22 CONTINUE
  22 GHYD(J+1)=QC*1000
   GO TO 8160
8140 GHYD(J+1)=C.
9160 CONTINUE
   GO TO 5150
-----END OF THE SUBPROGRAM DESIGN-----
C-----
C-----
C-----
C-----
SUBPROGRAM SIMULM ECLTES THE SEJER HYDROGRAPH CF LARGE RETURN
PERIOD ACCORDING TO THE PEAK DISCHARGE OF THE HYDROGRAPH
SUBROUTINE SIMULM
DIMENSION GHYD(250)
COMMON/TETA/UTPA,DCWNA,PIPEW,CANALN,L,TYPEA(4,2C),IJKL,IROUTE,ISTEP
COMMON/SIGMA/ALEN,DELTA
COMMON/GAMA/ALEN,DELTA
COMMON/RFO/EHYC(25C)
COMMON/CCI/NSSEC
SLCPE=(CEA-DCWNA)/ALEN
IF(IROUTE.NE.0) GO TO 1010
BIG=EHYD(1)
DO 1000 I=2,IJ*
IF(EHYD(I).GT.BIG) BIG=EHYC(I)
BIG=BIG/1000
IF(NSSEC.EG.1) GO TO 1130
1005 DEL=
AF=3.141593*(D/1000)**2/4
QF=AF*(C/4000)**(2./3)*SQRT(SLOPE)/PIPEN
IF(IROUTE.NE.0) GO TO 1020
QR=BIG/333*QR+C.2237778
DR=Q.67322*(1.-2*DR)
TH=2*ARCCS(1.-2*DR)
AR=(TH-SIN(TH))/6.282185
V=BIG/AR/AF
1.....2.....3.....4.....5.....6.....7.....8

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METU1041  
METU1042  
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METU1075  
METU1076  
METU1077  
METU1078  
METU1079  
METU1080

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.....1.....2.....3.....4.....5.....6.....7.....8
1990 IT=ALEN/V/DELT/60+1
      K=IJK-IT
      IF(K.LT.1) K=1
      DO 2000 N=1,K
      EHYD(IJK-M+1)=EHYD(K-M+1)
      DO 2010 M=1,IT
      EHYD(M)=C.
      RETURN
1130 QF=TYPEA(2,L)*SQRT(SLOPE)/CANALN
      RE=TYPEA(1,L)
      CALL YNCRMTYN,EIG,CANALN,SLOPE,8,0.7
      Y=YN
      A=Y*TYPEA(1,L)
      V=RIG/A
      GO TO 1350
1010 ARA=DELT*30/ALEN
      CC=0.
      A=C.
      IF(NSEC.EG.1) CC TC 7130
      GO TO 1030
1020 DO 5140 J=1,IJKL
      IF(EHYD(J).EG.C.C.AND.FHYD(J+1).EQ.0.0.AND.CC.LT.0.0001)GO TC 5145
      XX=(EHYD(J+1)-EHYD(J))/ISTEP/2000
      YY=(EHYD(J))/1000
      DO 200 I=1,ISTEP
      DELTAP=ARA/ISTEP*(YY+XX-CC)
      AP=A+DELTAP
      IF(AP.LT.C.) AF=0.
      AR=A/AF
      CR=1.037725*AR**1.388456
      IF(AR.GT.0.26)CR=1.075165*AR**1.413482
      QCB=QF*CR
      DELTAA=ARA/ISTEP*2*(YY+XX-QCB)
      AA=A+DELTAA
      IF(AA.LT.C.) A=C.
      IF(A/AF
      CR=1.037725*AR**1.388456
      IF(AR.GT.0.26)CR=1.075165*AR**1.413482
      CC=QF*CF
      YY=YY+2*XX
.....1.....2.....3.....4.....5.....6.....7.....8

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METU11082
METU11083
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METU11086
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METU11100
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METU11104
METU11105
METU11106
METU11107
METU11108
METU11109
METU11110
METU11111
METU11112
METU11113
METU11114
METU11115
METU11116
METU11117
METU11118
METU11119
METU11120

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.....1.....2.....3.....4.....5.....6.....7.....8

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20 CONTINUE
   GHYD(J+1)=CC*1CCC
   GO TO 5140
5145 GHYD(J+1)=C.
5150 CONTINUE
   DD 5160 J=1,IJK
5160 EHYD(J)=GHYD(J)
7130 RETURN
   B=TYPEA(I,I)
   DD 7160 J=1,IJKL
   YF(EHYD(J))-EQ.C.O.ANC.EHYD(J+1).EQ.0.0.ANC.CC.LT.0.0001)GC TO 7140
   XX=(EHYD(J+1)-EHYD(J))/ISTEP/2000
   YY=(EHYD(J))/1000
   DD 21 I=1,ISTEP
   DELTAP=ARA/ISTEP*(YY+XX-GC)
   AP=A+DELTAP
   IF(AP.LT.C.) AF=C.
   QCB=SQRT(SLOPE)/CANALN*AP**(5./3)*(B/(B**2+2*AP))**(2./3)
   DELTA=ARA/ISTEP*2*(YY+XX-GCB)
   A=A+DELTA
   IF(A.LT.C.) A=C.
   QC=SQRT(SLOPE)/CANALN*AP**(5./3)*(B/(B**2+2*A))**(2./3)
   YY=YY+2*XX
21 CONTINUE
   GHYD(J+1)=CC*1CCC
   GO TO 7160
7140 GHYD(J+1)=C.
7160 CONTINUE
   GO TO 5150
END
-----
C-----END OF THE SUBPROGRAM SIMUL
C-----
C-----
C-----SUBPROGRAM YNCRM CALCULATES THE FLOW DEPTH IN RECTANGULAR AND
      TRAPEZOIDICAL CANALS BY ITERATION
      SUBROUTINE YNCRM(YN,C,XN,S,B,Z)
      Y=0.001
      YY=0.001
      DELY=0.1

```

METU1121  
METU1122  
METU1123  
METU1124  
METU1125  
METU1126  
METU1127  
METU1128  
METU1129  
METU1130  
METU1131  
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METU1158  
METU1160

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.....1.....2.....3.....4.....5.....6.....7.....8
102 YN =(IC*XXN)/(S*C;F))*(B+2*Y*(1+Z**2)**0.5)**C.6667)/((B+Z*Y)**
  *1.6667)*(Y**0.6667))
  DELTA=Y-YN
  IF(A35(DELTA).LT.0.CC1) RETURN
  IF(Y.CT.YN) GO TO 101
  YY=Y+DELY
106 GO TO 102
101 Y=YY
  DELY=DELY/10.
  GO TO 106
C-----END OF THE METU DESIGN WCCEL PROGRAM-----
  END
.....1.....2.....3.....4.....5.....6.....7.....8
METU11161
METU11162
METU11163
METU11164
METU11165
METU11166
METU11167
METU11168
METU11169
METU11170
METU11171
METU11172
METU11173
METU11174
METU11175

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The University assumes no responsibility about the correctness of the statements in this thesis.